FIELD BOOK

740

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURT HOUSE
CHARDON, O.
PHONE 250-X

TABLE FOR REDUCING PERCHES TO FEET AND INCHES.

PERCH	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH	FEET.
1	16 6 in.	21	3.46 6 in.	41	6.76.6 in.	61	10.06.6 in.	81	13.36 6 in.
2	33.0	22	3 63.0	42	6.93.0	62	10.23.0	82	13.53 0
3	49.6	23	3.79.6	43	7.09 6	63	10.39.6	83	13.69.6
4	66.0	24	3.96.0	44	7.26.0	64	10.56.0	84	13.86.0
5	82.6	25	4 12.6	45	7 42.6	65	10.72.6	85	14.02.6
6	99.0	26	4.29.0	46	7.59.0	66	10.89.0	86	14.19.0
7	1.15.6	27	4.45 6	47	7.75.6	67	11.05.6	87	14.35.6
8	1.32.0	28	4.62.0	48	7.92 0	68	11.22.0	88	14.52.0
9	1.48.6	29	4.78.6	49	8.08.6	69	11.38.6	89	14.68.6
10	1.65.0	30	4.95.0	50	8.25.0	70	11.55.0	90	14.85.0
11	1.81.6	31	5 11.6	51	8.41.6	71	11.71.6	91	15 01.6
12	1.98 0	32	5.28 0	52	8.58.0	72	11.88.0	92	15.18.0
13	2.14.6	33	5.44.6	53	8.74.6	73	12.04 6	93	15.34.6
14	2.31.0	34	5.61 0	54	8.91.0	74	12.21.0	94	15.51.0
15	2.47.6	35	5.77 6	55	9.07 6	75	12.37.6	95	15.67.6
16	2.64.0	36	5.94.0	56	9.24.0	76	12.54.0	96	15.84 0
17	2.80.6	37	6.10.6	57	9.40.6	77	12.70.6	97	16.00.6
18	2.97.0	38	6.27 0	58	9.57.0	78	12.87.0	98	16.17.0
19	3.13.6	39	6.43.6	59	9.73.6	79	13.03.6	99	16.33.6
20	3.30.0	40	6.60.0	60	9.90.0	80	13.20.0	100	16.50 0

MUNN CH 32
E,F & G ~~Brown~~ Rd
SEC. ~~X~~ BROWNS CORNERS ROAD
422 to AUBURN TWP. Pg 2-13
Newbury Line
Geauga County, O.
Twp Road Improvement.
1922
Munn Road → Sec G, H & I p 28

Property of Geauga County Surveyor's Office
Chardon, O.

S. R. Kenney
Surveyor

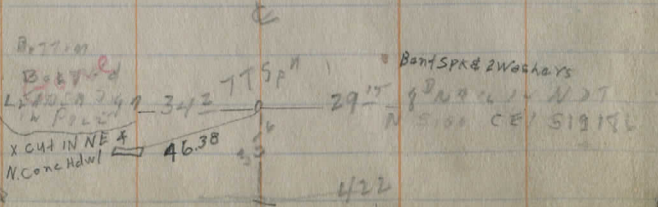
Harrys Cor. Road Newbury Twp (Browns Cor. North
T.H. 147
N+S Road past Geo. Munns Gravel Pit
Munn Road pg 28 to 39
C.H. #4
Magnetic Springs Road
Chardon Twp Pg 57

STAFFORD ROAD, AUBURN.
T.H. 187 Section ~~B~~ C & D pg 66
Brown Road Bridge Pg 49 A
STAFFORD Rd. Sec. ~~X~~. E & F
pg 10
OVER

Stafford Rd
Sec F

Pg 50

Sta.	Angle	Bearing
11		
10		
9		
8		
7		
6		
5	note: Changes in references made 1.934	
4		
3		
2		
1		
0		



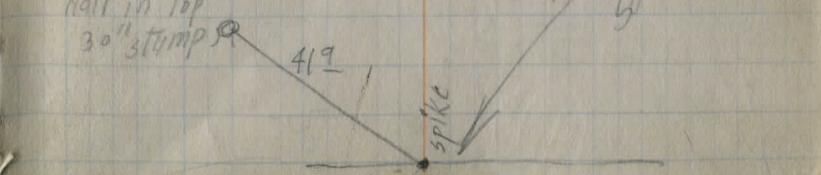
11-21-'22
cold
cloudy

Brown Rd
Sec. E

Hanna
Gray
Spann

offset stakes are set 20' to Rt. unless otherwise noted.

Note- This survey is merely a location for CTR of gravel and not on actual surveyed line of the road. G.R.H.



Note: new intersection on Browns Corners South see field notes.

23

+118 0°-19' Rt. I. P int Set 6-23-48

22

21

20

19

18

17

16

15

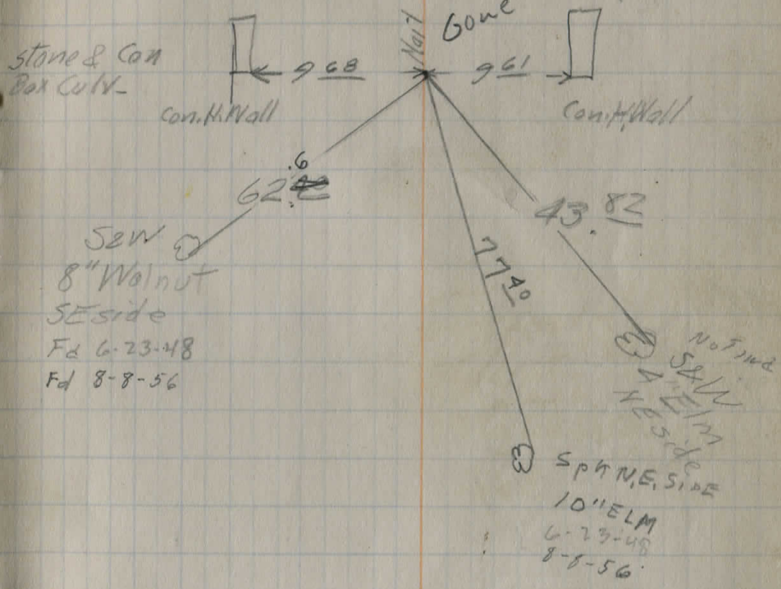
14

13

12

culvert replaced with
24" Cor. I.P. 30' long.

When New Culvt put in



Offset 20' Lt.

P.I. to P.I.5

c

1 09 N at Messenger

P.C. = 13+66.69		
14+0 — 33.31	0-10	1-54-30
15+0	0-40	1-44-30
16+0	1-10	1-14-30
17+0	1-40	0-44-30
PT +48.36	1-54 30	0-14-30

Curve deflection P.I. 15+57

36

35

34

33

32

31

30

29

28

27

26

25

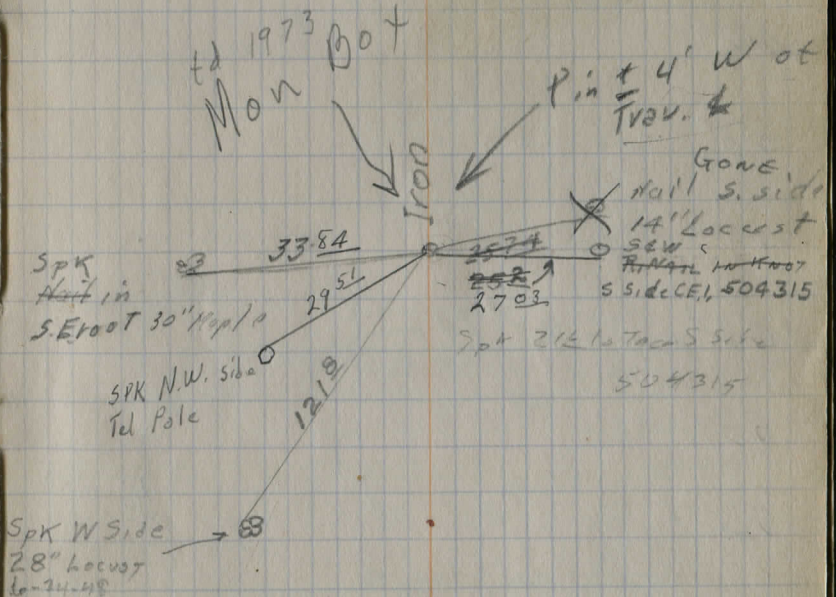
24

121.8

48
47
46
15
44
43
42
41
40
39
38
37

+31.7 0°-34' Rt.

1/2" I. Pin
Fd 6-24-48
10" Down



2161.20 Back from 7845.50 or 56+84 30

59

58

57

+85.0 △ 0°-0' △ 1½" I.P. PQT.

56

55

54

+01.0 ▲ 0°-38' Lt. I PIPE SET 6-24-48

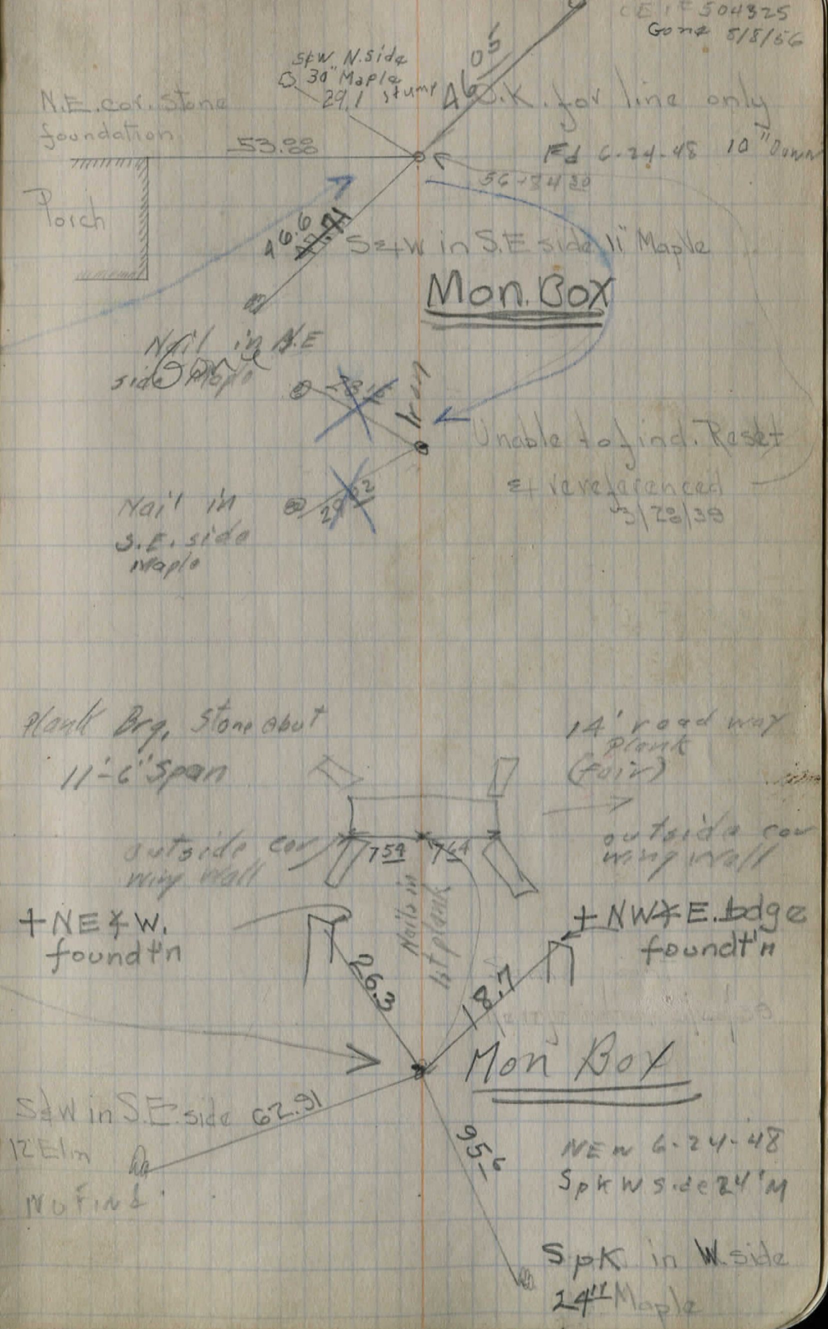
53

52

51

50

49



Spk SE
CE IF 504325
Gone 5/8/56
S&W N.side 30" Maple stump
29.1
0.5
46
N.E. cor. stone foundation
53.88
O.K. for line only
Fd 6-24-48 10" Down
56+84 30
Porch
46.6
S&W in S.E. side 11" Maple
Mon. Box
Nail in N.E side Maple
Unable to find. Reset & rereferenced 3/28/39
Nail in S.E. side Maple
Plank Brg, Stone abut
11'-6" span
14' road way plank (Fair)
outside cor. wing wall
outside cor. wing wall
7.59
7.64
Nails in 1st plank
+ NE & W. found'n
+ NW & E. Edge found'n
26.3
18.7
Mon Box
S&W in S.E. side 62.91
12 Elm
No Find
95.6
New 6-24-48
Spk W side 24" M
Spk in W. side 24" Maple

72

71

70

69

68

67

66

65

64

63

62

61

60

84

83

82

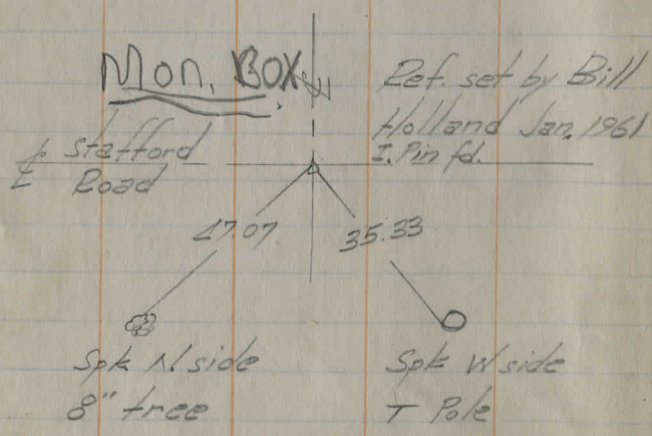
81

80

N. 5°-0' E.

79

+45 5/8 0°-17' Rt. I.P.



78

77

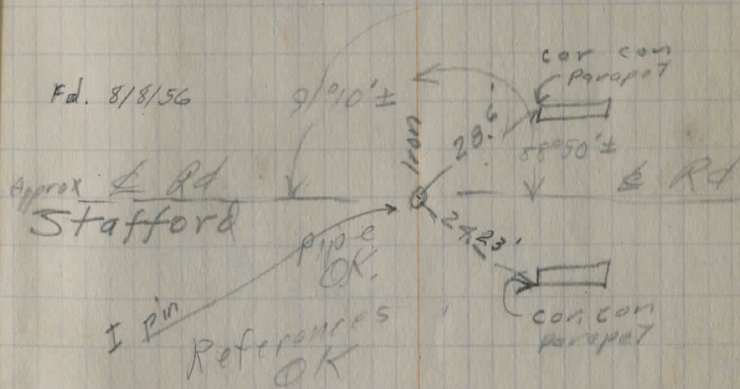
76

75

74

73

Brown Road
now MUNN
S¢C E & F



96

95

94

126.7

+73 3/0 0° - 31' Lt.

93

92

91

90

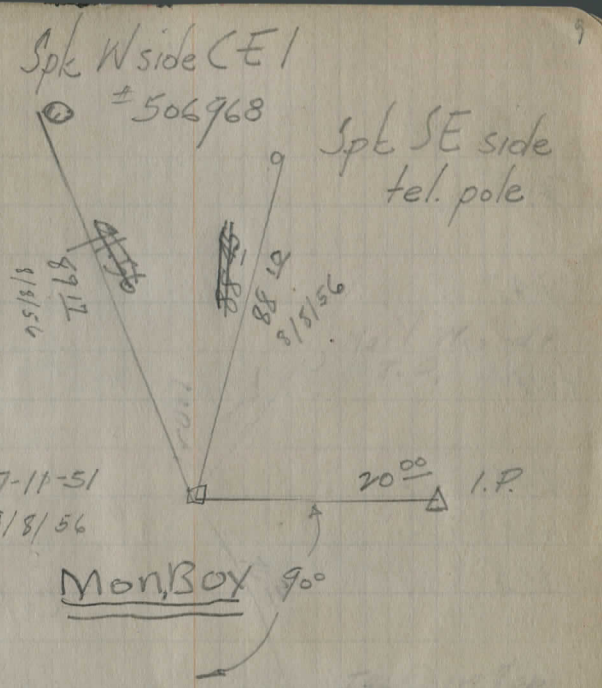
89

88

87

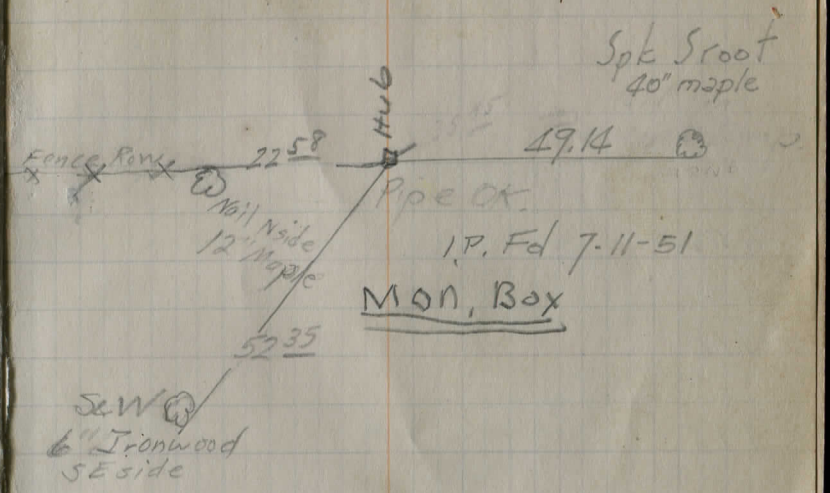
86

85



+11 P.T.
108
107
+61 Δ 12°-02' Rt.
106
+10 P.C.
105
104
103
102
101
100
99
98
97

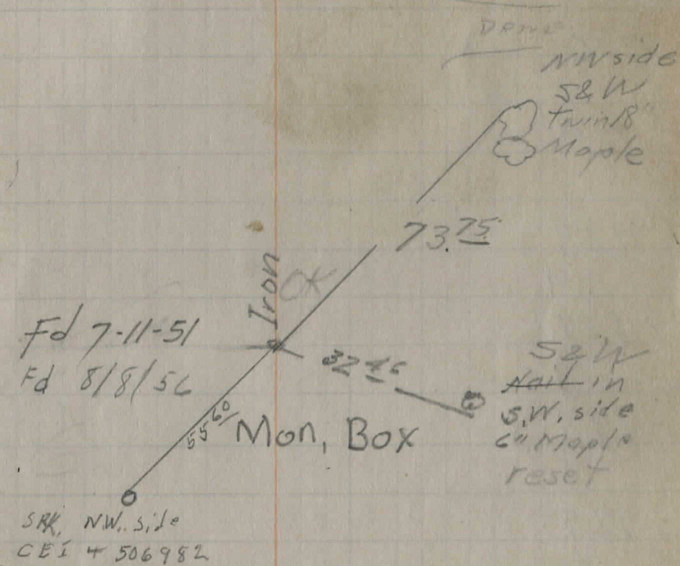
Δ = 12° 02' Rt.
D = 4° 00'
P.I. = 106 +61
T = 1 50
P.C. = 105 102
L = 3 00
P.T. = 108+11
E. = 7 ft.
R = 1432.40



10811
10700
111

+12
120
119
118
117
116
115
+79[4] ⊙ 1°-29' Rt
114
113
+26 MAN MADE DITCH FOR RUN OFF CUL. AT 111+46
112
+46
111
110
109

18" V.S.P. 31' | 17' | 14' | EXT. EAST



←

10" V.S.P. 76' | 15' | 11' | EXT ON EAST

133

132

131

130

129

128
+19

7' WEST END Broken

12" CastIron 26'

12' 14'

STINKER

127

126

125

124
+05

OK

24" Conc Pipe 33'

15' 18'

STINKER

123

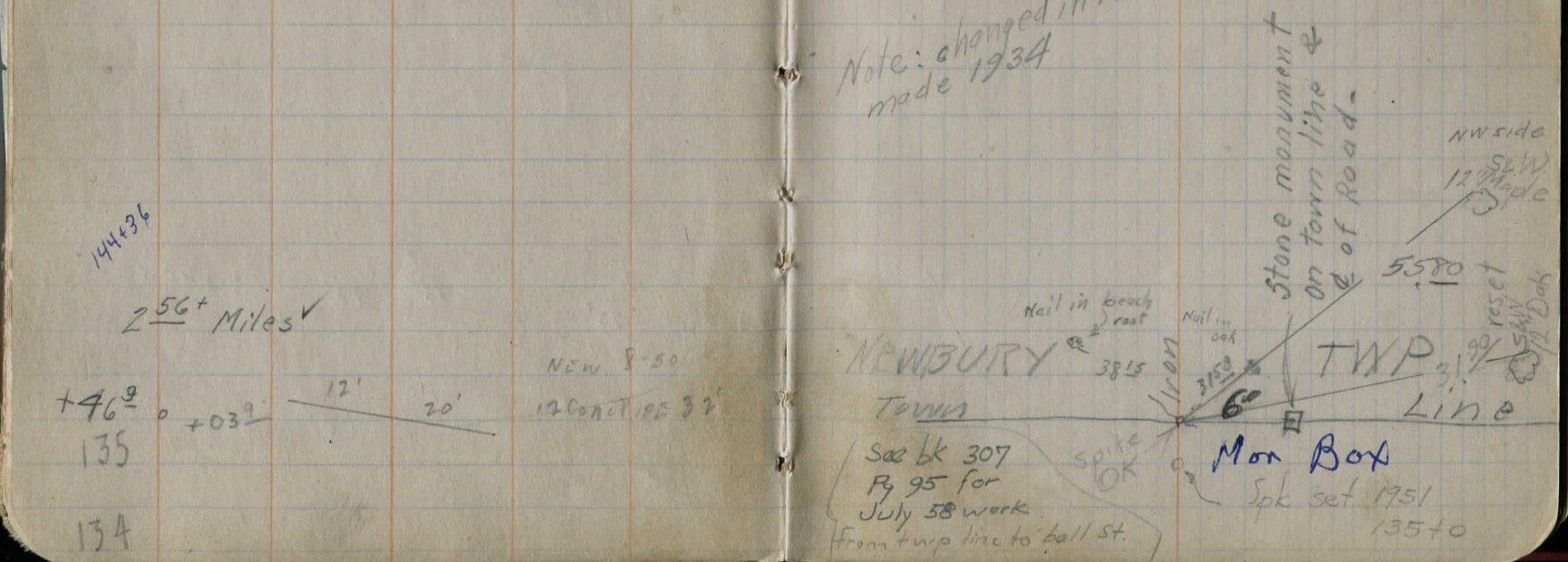
122

F. DIETZ

121

13547

Note: changed in references made 1934



Town Line
135+46 ℄

W. Davis

L. Shackson

127+62 P.I.

H 150' 127+0

W. Davis

P.I. 124+05

120+91 Road

H 100' 124+5[illegible]

B 75' 121+05

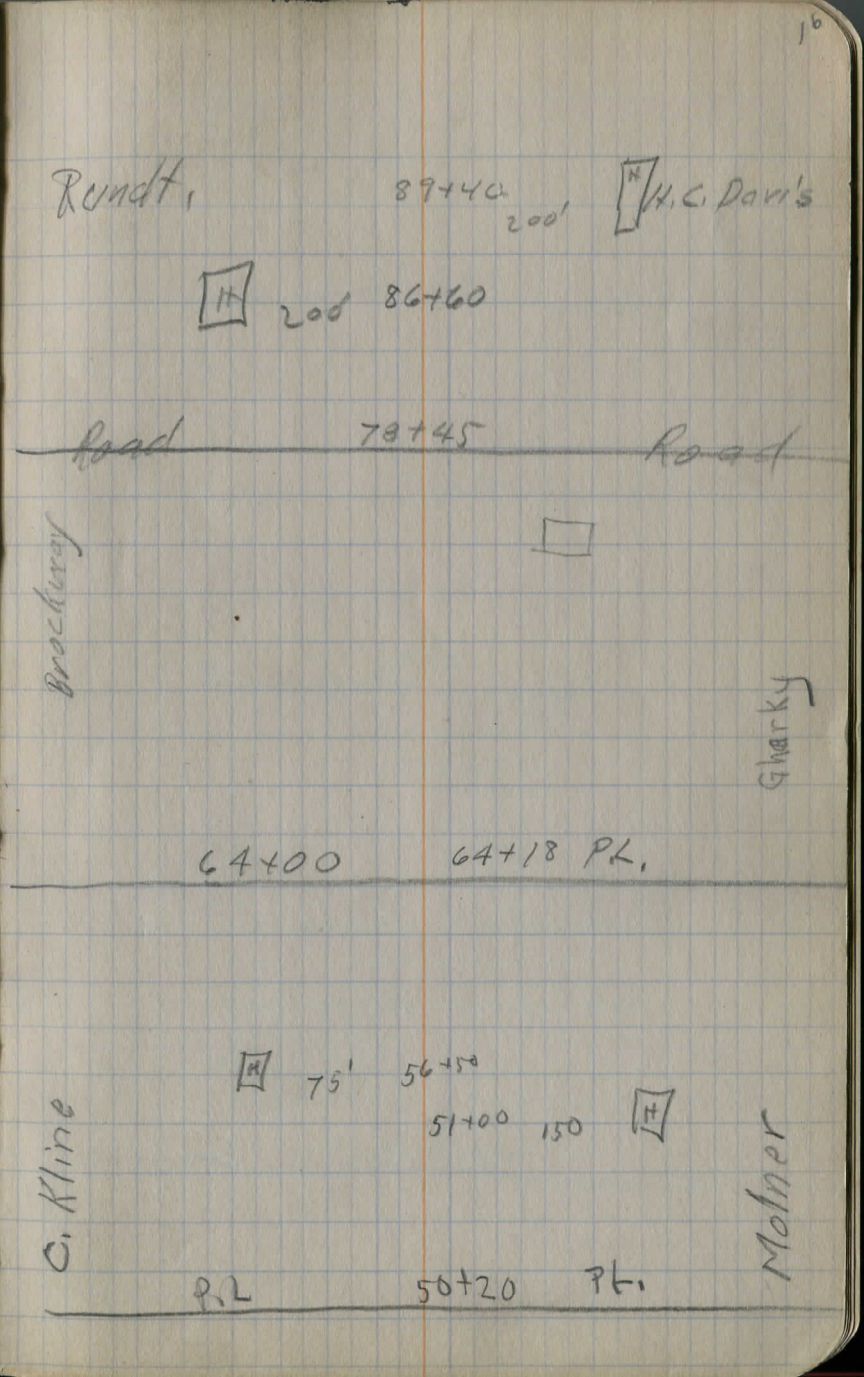
116+15

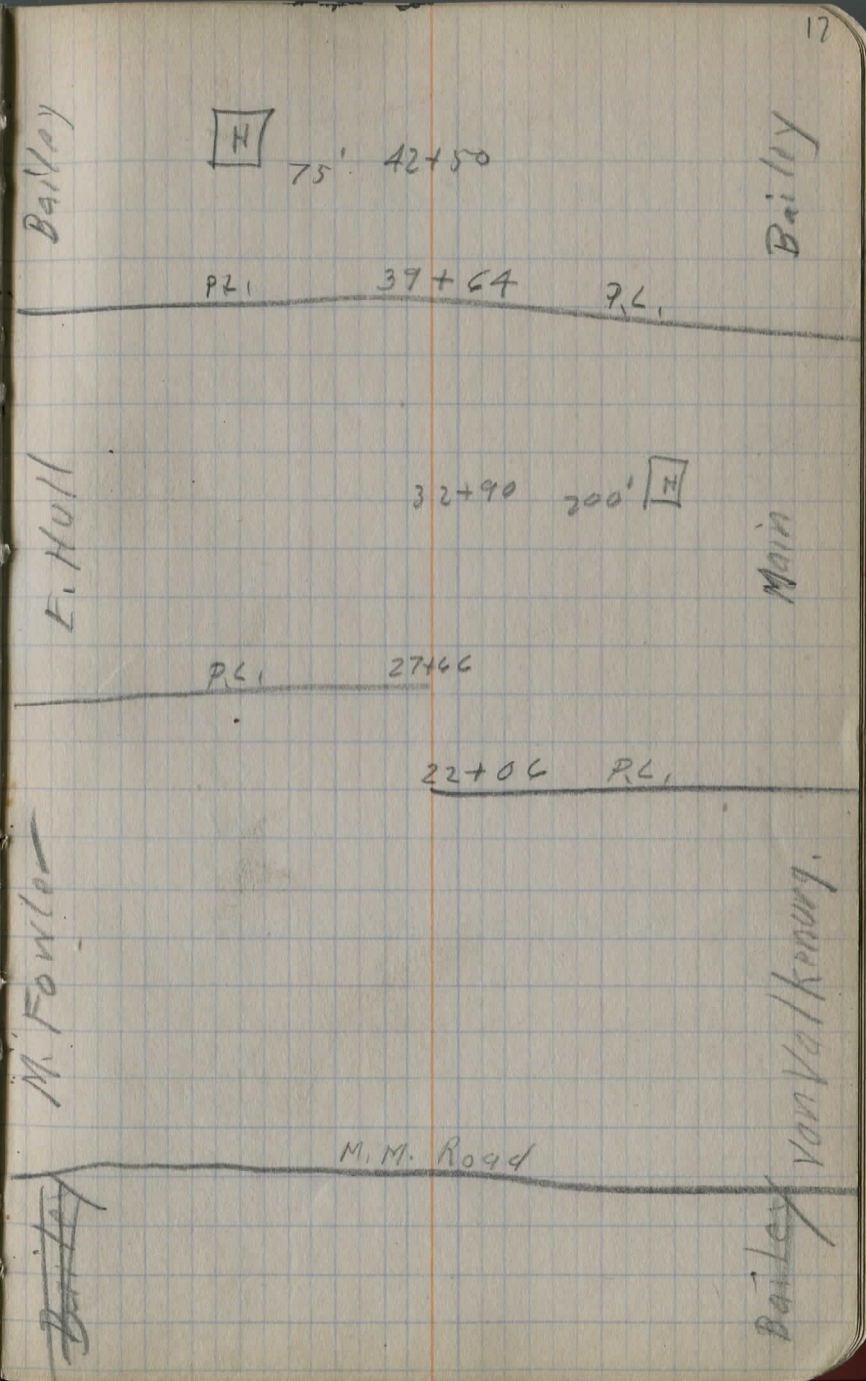
H 150

L. Shackson

J. Jackson

P.I. 106+61 P.C.

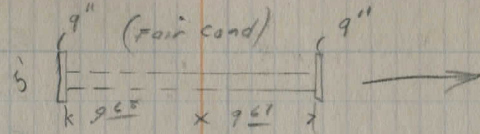

Rundt.
89+40
200'
H.C. Davis
200
86+60
Road
78+45
Road
Brockway
Gharky
64+00
64+18 PL.
75'
56+50
51+00
150
C. Kline
Mohler
R.L
50+20
PL.

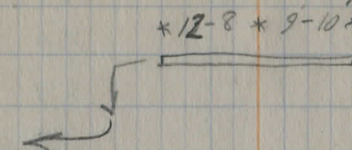

H
75'
42+50
Bailey
Bailey
P.I.
39+64
P.C.
E. Hull
32+90
200'
H
Main
P.C.
27+66
22+06
P.C.
M. Fowler
M. M. Road
Van Valkenburg.
Bailey

Sta	B.S.	H.I.	F.S.	Elev.	
B.M.	5.25	1167.06		11.61.81	S.W. Cor. S. Par. Con H. Wall - Culv. on M.M.Rd.
0			5.7	61.4	edge Con. Par.
1			5.8	61.3	
2			5.6	61.5	
3			5.3	61.8	
4			5.5	61.6	
5			5.0	62.1	
6			4.6	62.5	
7			4.0	63.1	
8			3.5	63.6	
9			3.2	63.9	
10			3.1	64.0	
11			3.5	63.6	
12			3.4	63.7	
13			3.6	63.5	
T.P.	0.94	1166.42	1.58	1165.48	2 nails in E. Root Maple E. root 13+25
14			2.3	64.1	
15			2.5	63.9	
16			3.0	63.4	
17			4.0	62.4	
18			4.9	61.5	
19			5.2	61.2	
20			5.5	60.9	
21			5.6	60.8	
22			5.8	60.6 ✓	

		1166	42		
T.P.	4.58	11.66	17 con- cover	4.83	1161.59
22+13				5.9	60.3
23				5.8	60.4
24				5.7	60.5
25				4.9	61.3
26				4.1	62.1
27				3.7	62.5
28				2.7	63.5
29				0.8	65.4
T.P.	5.47	1170	53	1.1	1165.06
30				4.1	66.4
31				4.4	66.1
32				3.8	66.7
33				4.1	66.4
33+85 14" C.I.P.					
34				4.0	66.5
35				3.8	66.7
36				3.5	67.0
37				3.4	67.1
38				3.1	67.4
39				2.5	68.0
40				2.3	68.2
T.P.	6.23	1174	75	2.01	1168.52
41				5.4	69.3

W. Par-
4 × 3½ Stone
& Con Culv.

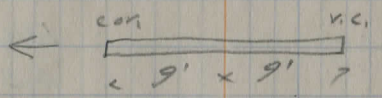


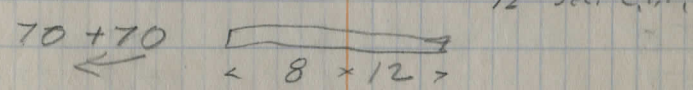


Good cond

		1174	75			
42				4.2	70.5	
+30				3.8	70.9	
43				4.0	70.7	
B.M.				0.97	1173.78	S.E. Cor. 1st Con. ~~3rd~~ Step of Con. Steps to house Lt.
44				4.4	70.3	
45				4.1	70.6	
46				3.5	71.2	
47				3.0	71.7	
48				2.0	72.7	
49				1.2	73.5	
+35				1.5	73.2	Rt. Bank begins
50				3.1	71.6	3' Bank Rt.
T.P.	0.99	1173	14	2.60	1172.15	
51				4.7	68.4	Bank on Rt. ends 51+50
52				7.0	66.1	
+50				6.9	66.2	
53 + floor				4.5	68.6	Brg. floor
B.M.				4.36	1168.78	X on S.E. Cor Rt. Wing S. Abut
				11.4	61.7	Bot. creek
+30				5.8	67.3	14' Roadway 2' Fill
54				5.8	67.3	
+50				5.1	68.0	
55				2.8	70.3	
T.P.	10.74	11 81	55	2.33	1170.81	
56				5.8	75.7	22' Ditch — dry

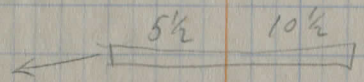
		1181	55		
57			2.8	78.7	19' d-d
+60			1.8	79.7	17' d-d
58			3.1	78.4	17' d-d
59			5.1	76.4	
+50	12" V.P. & Cor		5.4	76.1	
60			5.0	76.5	
61			3.8	77.7	
62			2.3	79.2	
T.P.	8.89	1188	02	2.42	1179.13
63				5.9	82.1
64				3.9	84.1
+80				3.6	84.4
65				4.3	83.7
66				4.6	83.4
67				4.1	83.9
68				3.7	84.3
69				5.3	82.7
70				5.7	82.3
71				5.1	82.9
72				4.1	83.9
T.P.	7.95	1191	66	4.31	1183.71
73				6.8	84.9
74				5.9	85.8
75				4.8	86.9
76				3.4	88.3
77				1.1	90.6 ✓





		1191	CC			Hanna Grau Spohn	11-24-'22 Cold!!!!!! Snow Storm!!!
T.P.	10.10	1199.63		2.13	1189.53		
78				6.2	93.4		
B.M.	10.06	1208	63	10.6	1198.57	S.W. Cor S. Par. Con. Culv. on x Rd.	
+50				11.9	96.7		
79				10.6	98.0		
80				6.5	02.1		
~~81~~				0.6	08.0	17 d-d	3' bank Rt.
T.P.	12.47	1220	24	0.8	1207.77		
~~82~~				=		19' d-d	"
+35				9.4	10.8		
82				6.0	14.2	18' d-d	"
83				1.6	18.6		
+30				0.8	19.4		
T.P.	11.40	1231	51	0.13	1220.11		
84				8.5	23.0	18' d-d	"
85				5.0	26.5		
86				1.8	29.7	17' d-d	
T.P.	10.03	1242	21	0.13	1231.38		
87				9.8	32.4	20' d-d	1' bank Rt.
+90				6.9	35.3		
88				6.0	36.2		
89				2.7	39.5	5' bank Lt.	Level
T.P.	12p9	1254.22		0.08	1242.13		
90				10.6	43.6 ✓	4' bank 18' d-d	

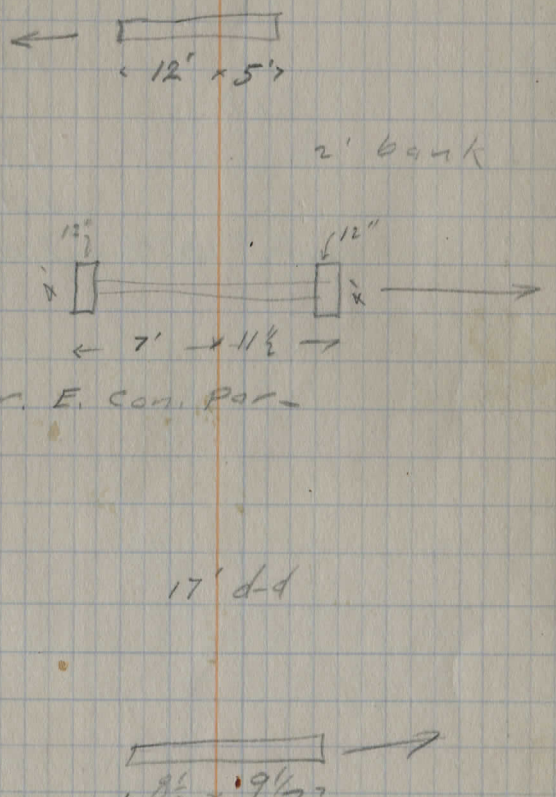
		1254	22					
+45				8.5	45.7			
91				5.0	49.2	5' bank	13½ d-d	3' bank
T.P.	10.17	1264	30	0.09	1254.13			
92				8.4	55.9	"		
+30	(?)(50)?			4.4	59.9	"		
93				3.2	61.1	1' bank	18' d-d	Level
+50				2.0	62.3	"		"
94				2.4	61.9	"	15' d-d	"
95				6.9	57.4	3'		2' bank
T.P.	0.91	1253	90	11.31	1252.99			
96				2.9	51.0	3' bank	16' d-d	3' bank
97				7.5	46.4	2' "		2' "
98				11.8	42.1	2' "		1' "
T.P.	1.26	1242	55	12.61	1241.29			
99				4.1	38.1	1½	17½	2' "
100				7.8	34.7			
B.M.				6.44	1236.11	Nail in E. root 36" Maple 30' Lt. 100+15		
101				12.3	30.2			
T.P.	0.79	1230	57	12.77	1229.78			
102				3.2	27.4	No bank	15' d-d	No bank
103				5.6	25.0			
+60	12" sec. C.I.P.				✓			



		1230.57				
104				7.5	23.1	about flat
T.P.	2.21	1225	14	7.64	1222.93	
105				3.8	21.3	
106				6.0	19.1	1' bank 1' bank
107				7.1	18.0	
+50				8.2	16.9	
108				8.5	16.6	
109				10.5	14.6	19' d-d
T.P.	2.70	1216	83	11.01	1214.13	
110				3.9	12.9	Level 20' d-d level
111				4.6	12.2	
+45	Plank box Reg. 12" pipe			4.4	12.4	← 8-C 8-C
112				4.2	12.6	
113				3.0	13.8	
114				1.4	15.4	
T.P.	6.80	1222	21	1.42	1215.41	
+65				4.6	17.6	
115				4.2	18.0	½' banks
B.M.				4.5	17.7	Nail S.E. root 48" Elm 36' Rt. 116+60
B.M.				3.03	1219.18	
117				5.8	16.4	
118				9.3	12.9	1' bank 15' d-d 2' bank

1222 21

119				13.0	09.2	Level 16' d-d 2' bank
T.P.	3.70	1213	26	12.65	1207.50	
120				5.0	08.3	slight fill slight fill
+06	20" V.P.					
	Lt end length broken-					
121				5.1	08.2	
122				3.0	10.3	2' bank
123				4.4	08.9	
+35	20" Corr. Pipe					
						Excellent Cond.
B.M.				3.12	1210.14	N. N.E. cor. E. Con. Par-
124				4.1	09.2	
+60				2.3	11.0	
125				1.9	11.4	
126				3.0	10.3	17' d-d
T.P.	4.72	1214	52	3.46	1209.80	
127				5.1	09.1	
+18	12" C.I.P.					
128				4.5	10.0	
129				3.1	11.4	20' d-d
130				2.8	11.7	20' d-d
131				2.5	12.0	

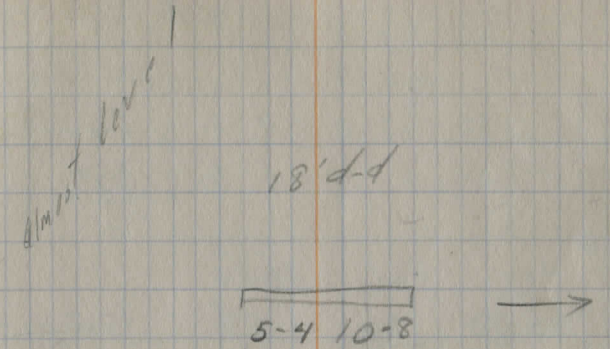


		1214	52		
132				1.1	13.4
T.P.	6.36	1219	02	1.86	1212.66
133				4.6	14.4
134				3.9	15.1
135				4.5	14.5
+03	10" Sec. C.I.R.				
+46.1				3.7	15.3
				1.4	17.6
B.M.			54	2.48	1216.51

✓

100' in Newbury

Nail in S.E. root 18" Beech - Lt.



+	Hi	−	12-5-53 Pam John Art
BM	4.28	Nov. 89	1198.61

Set at ± 32+47 & ± ℄ ang from ℄ E

All ang's turned to right

Set A BS ℄E	Ang	Rod	Stadia		
① stk	98-30	7.6	53′ 4.76	95.3	
② stk	109-30	7.6	130 4.50	95.3	
③ stk	111-06	7.3	210 5.38	95.6 ✓	
T.P.	3.02	1200.54 ✓	5.37	1197.52 ✓	
	111-11		327′		HUB B
④ BS on A	195-10	5.7	101 3.4	94.8 ✓	
⑤	197-02	6.0	260′	94.5 ✓	
	197-02	3.70	283		Hub C
T.P.	4.17	1201.01 ✓	3.70	1196.84 ✓	
BS on B					
	213-25	7.1	178′	93.9	
	211-05	7.2	260	1193.8 ✓	
	215-53	5.21	2.60		

Levels on outlet channel
Culvt Sta. 32+57 Stafford Rd
T.H. # 187 See E

NW ✱ N holw l

7.8 F/L H 95.1

7.4 F/L S 95.5 ✓

channel

Note: Channel is prob. man excavated (long time ago)

CHAN'L 5' WEST SAME ELV.

See Final grades pg. 53

± 40' SW of Ch. entering from E
= 3' NW of 1½' stone 12' SE of 12" Elm 40' NE or E of 24" Hick

3' E of ℄ Chan'l

Hi Point 2' ROCK 15' NW of Chan'l 'tween 3 BLAZED ELMS

8-8-24
Fair
Hot

Hanna
Sperry
Pomeroy

Sta	Angle	Bearing
11		
10		
9		
+ 91-8	△ 1°-21' Lt.	
8		
7		
6		
5		
4		N. 0°-05' E.
3		
2		
1		Magnetic
0		

SEE FD BK # 307 Pg 96 for '59 notes (Twp. line to Bell St.)

Aub- New TWP LINE

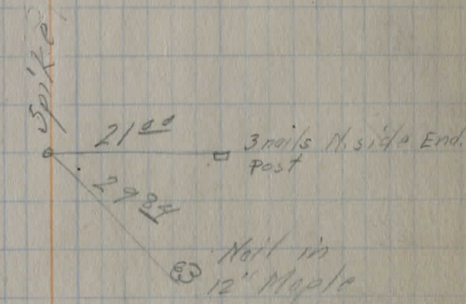
MUNN RD. Newbury Twp Road

North + South Road passing Munn's Gravel Pit.

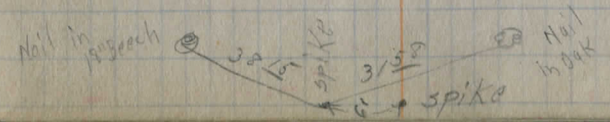
Harrys Cor. Road (Browns Cor. North)

Offset stakes set 20' Rt. unless otherwise noted.

~~Note:- This Survey is merely a location line for the ctr. of the gravel. And not an actual ℄ of the right-of-way~~



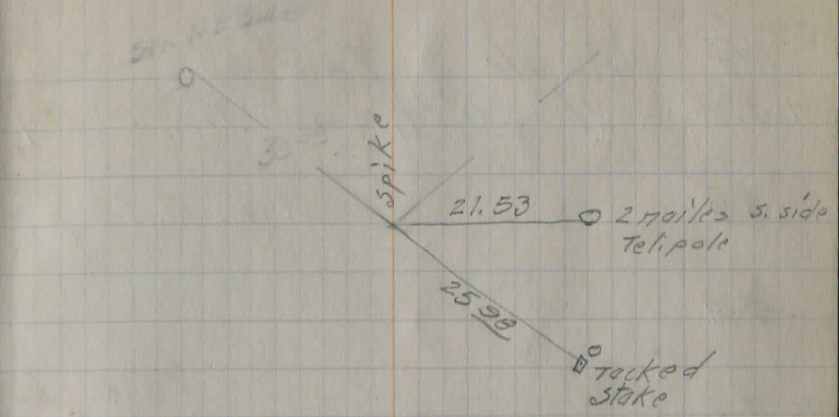
See Auburn Section for revised references set 3/6/34 pg 13

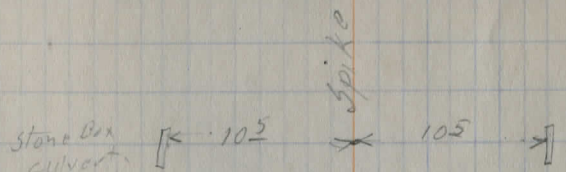


℄

Sta	Angle	Bearing
24		
23		
22		
21		
20		
19		
18		
17		
16		
15		
14		
13		
12		

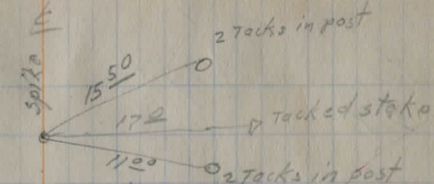
Sta.	Angle	Bearing
35		
+60 $\frac{6}{}$	Δ 1°-13' Rt.	
34		
33		
32		
31		
30		
+26 $\frac{2}{}$	Δ 0°-20' Lt.	
29		
28		
27		
26		
25		

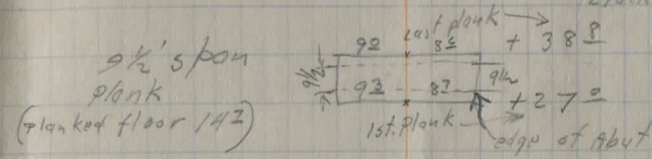


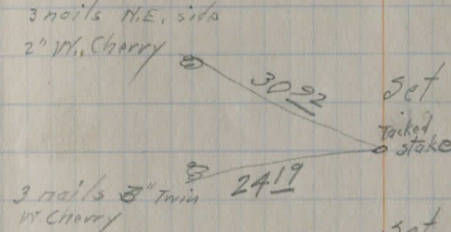


℄ Bell Street = Sta 28+

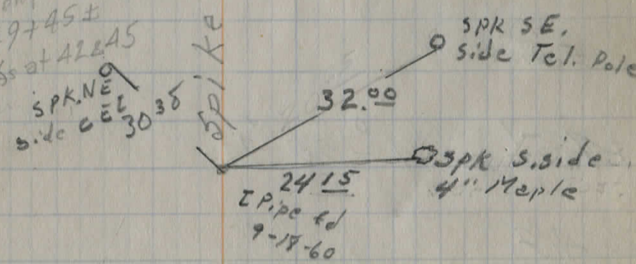
Sta	Angle	Bearing	
+35⁰	△ 11°-20' Lt.	set 17' Rt. of Tang	
45		set 19½' Rt. of Tang.	
44			
43			set 23' Rt. of Tang-
+94⁴	△ 10°-27' Rt.		
42			set 21½' Rt of Tang-
41			
40			
+05²	△ 2°-30' Rt.		
39			
38			
37			
36			







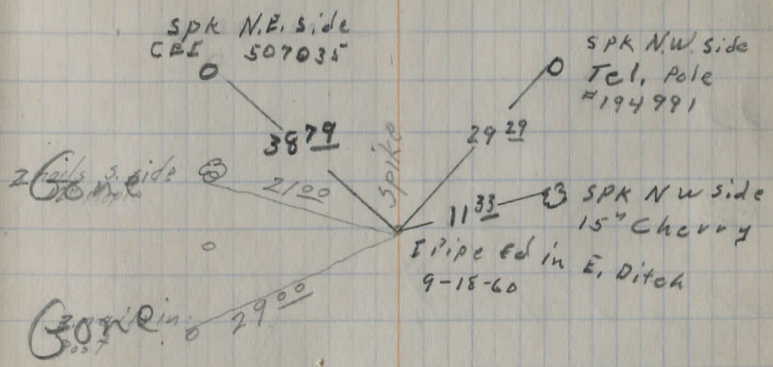
6/10/36
Made tangent from
37+05± to 49+45±
Eliminated △s at 42 & 45



Hanna
Sperry
Pomeroy

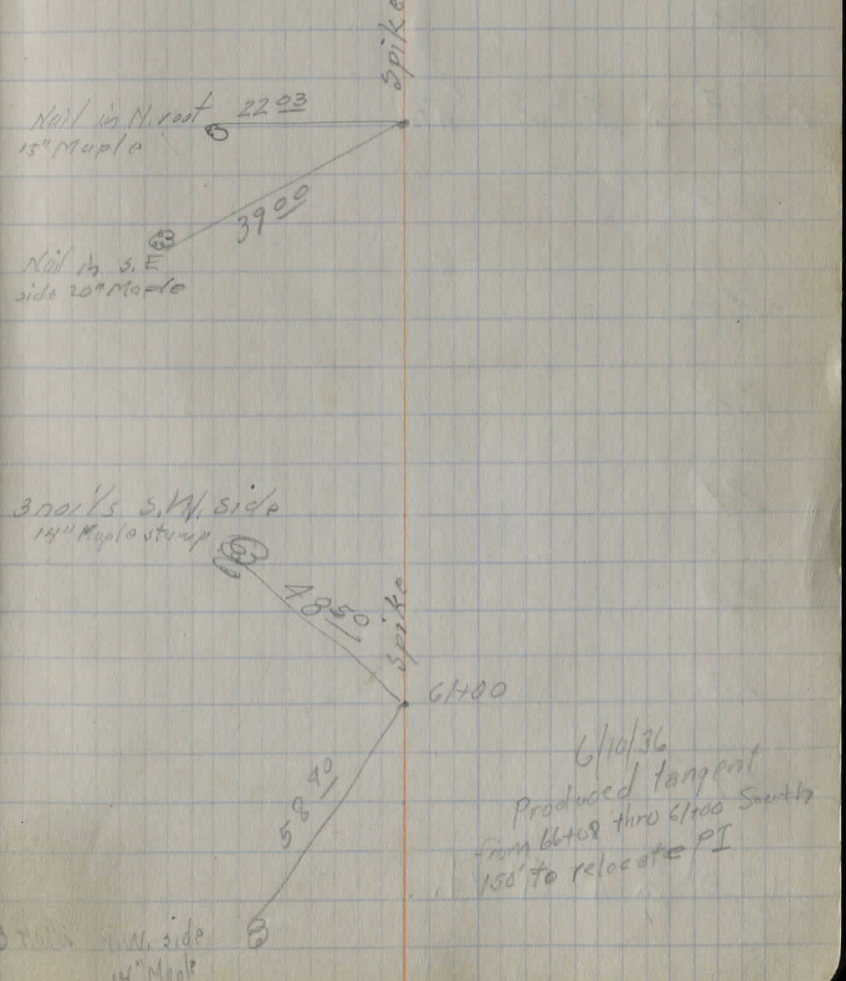
8-11-'24
Rain

Sta.	Angle	Bearing
57		
56		
55		
54		
53		
52		
51		
50		
~~+45~~ 45.7	Δ 4° - 55' Lt.	
49		
48		
47		
46		



Set 19' Rt of Tan

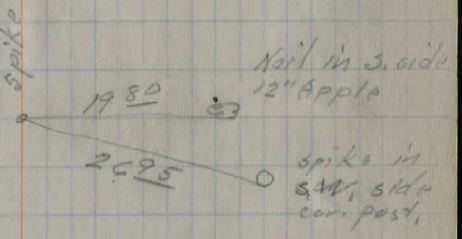
Sta	Angle	Bearing
69		
68		
67		
+08 ∘ 4°-56' Lt.		
66		
65		
64		
63		
62		
61 ∘ 2°-46' Lt.		
60		
59		
58		



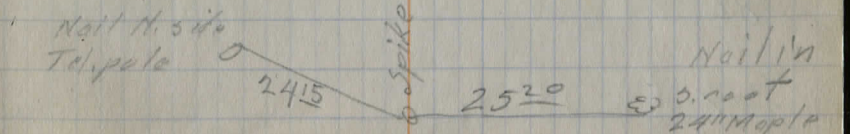
Sta	Angle	Bearing
80		
79		
78		
+23.5	△ 2°-23' Rt.	
77		
76		
75		
74		
73		
72		
71		
+20.1	△ 4°-21' Lt.	
70		

Note:- ℄ Music Street = Sta 80 ±

Set 21' Rt. of Tang.



6/10/36
Set PI 25' Lt of 1st Tree N of S. Drive of Geo Monn's at Sta 70+20 ± Made tangent from 70+20 to Sta 80



Sta	Angle	Bearing
92		
91		
90		
89		
88		
87		
86		
85		
84		
83		
82		
81		

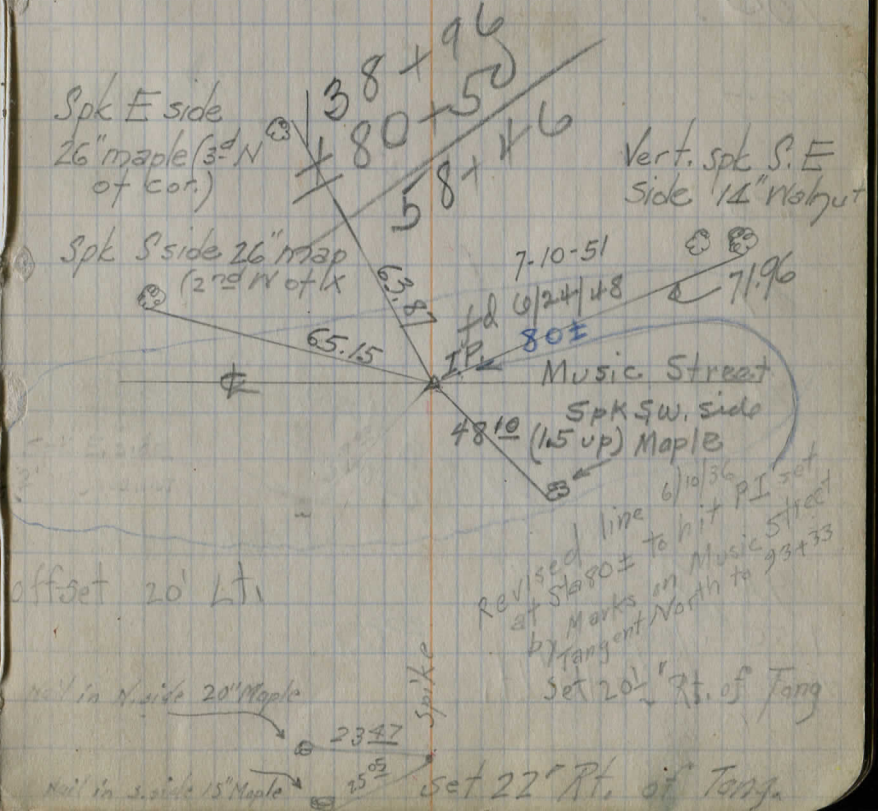
+ 37.7 Δ 12° 31' Rt.

OFFSET STAKES SET
15' EAST OF ℄ UNLESS MARKED
OTHERWISE 6-29-48
START AT MUSIC 0+00

32+00 = 13'

8+0 - 9+0 prob Fr dr in
but needs ditches

6+40 - +70 Fr. dr
reqd



8-12-24
Hot.

Hanna
Sperry
Pomeroy

Sta | Angle | Bearing

109
108
107
106
105
104
103
102
101
100
99
98
97
96
95
94
93

107+79

0°-07'

1446

2.9°

93+33

179+45

12 83

0°-08'

If using I.P. at ℄ Musis Street = 80+00

±80+50

℄ Music St

+50 6/24/48

+33 3 0°-15' Lt

P.O.T.

℄

Spike

26+0 - 26+70
Fr. dr. road
& ditches

5 & W - N.E. side
24" W. Cherry
53
56 Lt

5 & W - S.E. side
28" Maple
53
46 83

(in E. berm)
Spk P.O.T.
Music St
+01 10+53.94

Nail in N.E. side
8" Maple

21 40

Nail in S.E. side 10" Maple

26 05

Spike

could not find
6/10/56
No find

Sta. Angle Bearing

115

+84.34

+59 3 Δ 0°-26' Lt.

114

113

112

111

+53 94 Δ = 0-23 R (for tang. N. to Rt #87) IP set 6/25/48

110

109

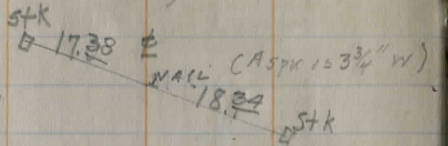
108

+79 6 Δ 0° ~~12'~~ Rt.

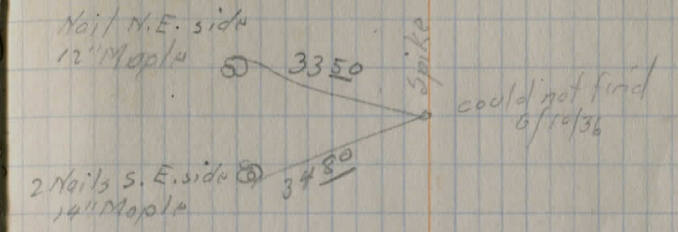
107

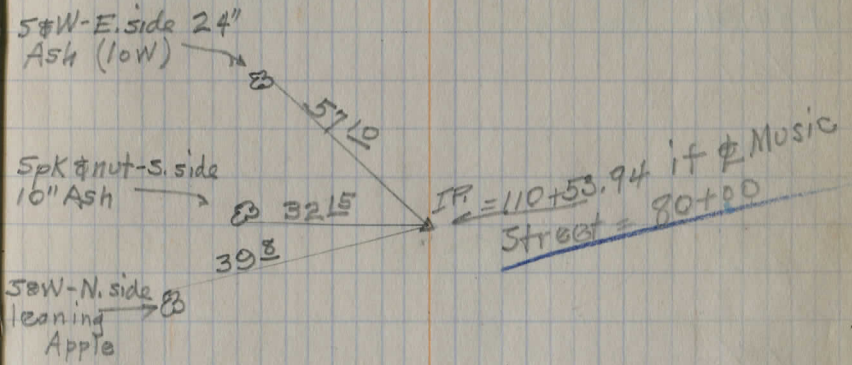
106

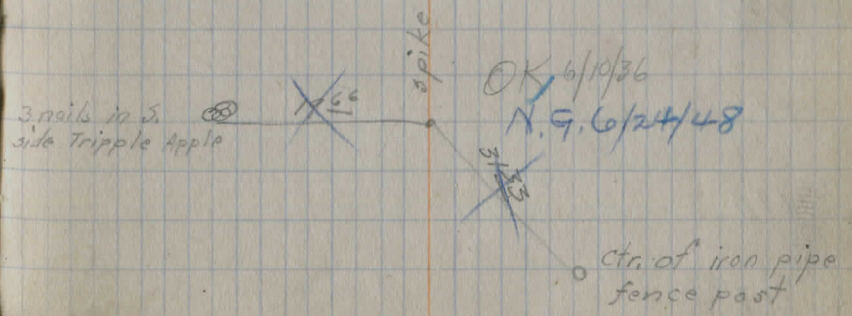
105



℄



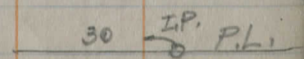




Sta.	Angle	Bearing
128		
127		
126		
125		
+84.34		
124		
123		
122		
121		
120		
119		
118		
117		
116		

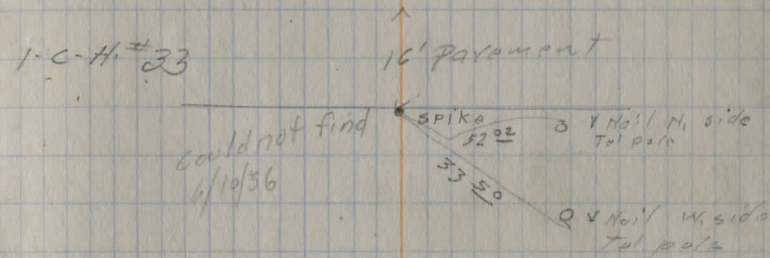
30 ∠ I.P. Prop.

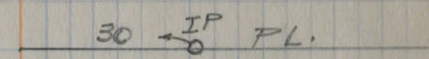
Sta	Angle	Bearing
139+11.44 = ℄ Rt. #87 it ℄ Music St = 80+00		
+88.4 △	The end	
138		
137		
136		
135		
+35.7		
134		
133		
132		
131		
130		
+60.0		
129 △	0°-0'	

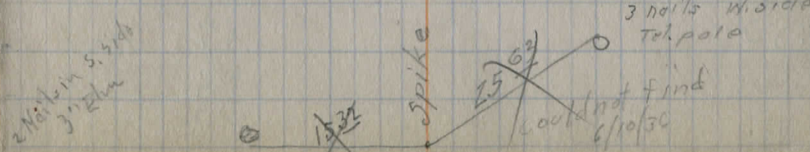


13911
80
5911

5911







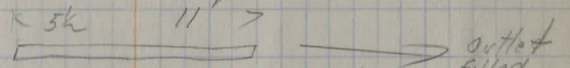
PROFILE LEVELS

P.M. 8-12-24
Fair-Fine

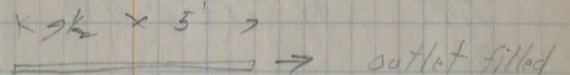
Hanna
Pomeroy
Sperry

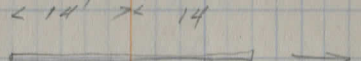
Sta.	B.S.	H.I.		F.S.	Elev.
B.M.	6.58	1223	12		1216.54
0				7.2	15.9
1				5.6	17.5
2				3.3	19.8
3				4.1	19.0
4				4.8	18.3
+08	℄ 12" C.I.P.			5.0	18.1
5				3.8	19.3
6				1.6	21.5
T.P.	11.75	1232	93	1.94	1221.18
7				7.8	25.1
+65				5.7	27.2
8				5.0	27.9
9				3.5	29.4
+50				3.1	29.8
10				3.7	29.2
11				6.2	26.7
12				7.7	25.2
13				8.6	24.3
14				10.2	22.7
T.P.	0.27	1223	09	10.11	1222.82
15				3.5	19.6
+30				4.7	18.4
16				8.4	14.7
17				14.4	08.7

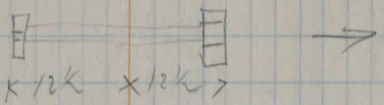
Fair



		1223 09			
T.P.	0.51	1210.82	12.78	1210.31	
18			5.1	05.7	
19			6.9	03.9	
+64	℄ 12" C.I.P.		8.0	02.8	Fair
20			8.2	02.6	
21			6.9	03.9	
22			6.0	04.8	
23			4.8	06.0	
24			5.5	05.3	
T.P.	1.23	1206.15	5.90	1204.92	
25			1.9	1204.3	
26			3.7	1202.5	
27			5.3	1200.9	
+48	℄ 10" C.I.P.		6.7	1199.5	Good
+78	℄ X Rd		7.1	1199.1	
28			8.1	1198.1	
29			8.5	1197.7	
B.M.			6.43	1199.72	S.W. Cor Parapet stone Culvert 29+26
29+26	℄ 3×3 Stone Box		8.6	1197.6	O.K.
30			9.2	1197.0	
31			9.6	1196.6	
32			10.0	1196.2	
33			11.1	1195.1	
T.P.	1.56	1196.87	10.84	1195.33	
34			5.4	1191.9	
35			9.2	1187.7	







(CALC '79)

		1196	87			
36				11,0	1185.9	
37				12,6	1184.3	
T.P.	1.41	1185	40	12.88	1183.99	
38				2,5	1182.9	
39				4,1	1181.3	
40				9,2	1176.2	
T.P.	1.50	1173	91	12.99	1172.91	
41				7.7	1166.2	
T.P.	0.46	1161	79	12.58	1161.33	
42				4.5	1157.3	
43				8.3	1153.5	
44				10.7	1151.1	
+32				10.8	1151.0	Bridge floor. 9k clear span
B.M.				10.35	1151.47	S.E. Cor Rt. wing S. Abut.
45				11.9	1149.9	S.L
+35				10.2	1151.6	
46				4.9	1156.9	
T.P.	11.41	1162	81	10.39	1151.42	
47				6.4	1156.4	
+60				0,5	1162.3	
T.P.	10.13	1172	42	0,52	1162.29	
48				7.5	1164.9	
+50				4.8	1169.6	
49				3.2	1169.2	
+40				2.6	1169.8	
50				5.3	1167.1	

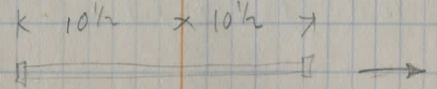
8-14-24 Fair Hanna Sperry

(Calc'd)

		1172	42		
51				7.1	1165.3
52				8.7	1163.7
S.P. B.M.	12.45	1176	17	8.70	1163.72
53.	No culvert.			11.5	1164.7
54				9.7	1166.5
+50				8.9	1167.3
55				6.4	1169.8
+30				5.0	1170.2
56				4.1	1172.1
57				1.4	1174.8
58				0.0	1176.2
T.P.	10.78	1186	83	0.12	1176.05
59				7.5	1179.3
60				4.2	1182.6
+75				4.0	1182.8
61				4.6	1182.2
+80				5.9	1180.9
62				7.3	1179.5
+40				9.6	1177.2
T.P.	0.58	1175	01	12.40	1174.43
63				2.7	1172.3
64				8.2	1166.8
65				10.0	1165.0
+52 & 3 x 3½ stone			fair	11.0	1164.0
64				11.2	1163.8

Spike in E. side dead elm 4ft. 52+80

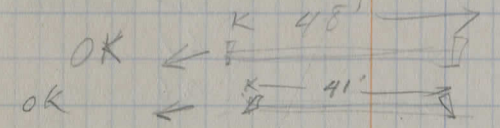
(will do).

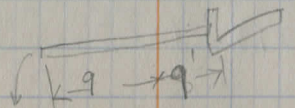


(CALC '79)

		1175 01		
67			10,7	
T.P.	10,81	1175 01	10,81	1164.20
68			8,7	1166.3
69			7,7	1167.3
B.M.			1.38	1173.63
70			3,1	1171.9
71			1,8	1173.2
72			-0,3	1175.3
T.P.	11.61	1185 89	0.73	1174.28
73			7,3	1178.6
74			6.9	1179.0
75			6.7	1179.2
76			4,9	1181.0
T.P.	9.49	1195.39	-.01	1185,90
77			7.2	1188.2
+30			5.5	1189.9
78			4.5	1190.9
79			8,2	1187.2
+65	℄ 1½ × ½ stone Box		8,5	1186.9
80+00	℄ 1½ × ½ stone Box		8,7	1186.7
81			8.0	1187.4
82			5,0	1190.4
T.P.	10.11	1202 14	3.36	1192.03
+33			10.1	1192.0
83			7.3	1194.8
84			2.3	1199.8

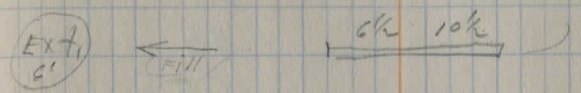
+ 5.W cor Stepping stone front of Mona's house

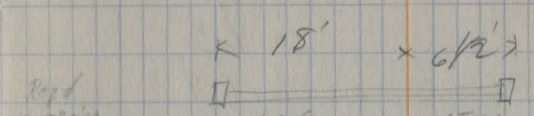


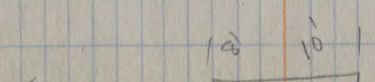


(CALC '79)

		1202	14		
T.P.	11.67			0.17	1202.07
~~85~~				8.7	1193.4
+65	℄ 10" C.I.P.			8.4	1193.7
86				8.0	1194.1
87				4.6	1197.5
T.P.	9.26	1211	20	0.20	1201.94
88				5.9	1205.3
+60				~~4.5~~	1206.9
89				5.5	1205.7
+75				7.5	1203.7
90				6.8	1204.4
+45	℄ 1'-3" x 1'-6"			7.8	1203.4
91				6.2	1205.0
T.P.	12.68	1222	62	1.26	1209.94
92				10.6	1212.0
+50				6.6	1216.0
93				4.6	1218.0
94				2.5	1220.1
95				1.1	1221.5
96				0.6	1222.0
97				2.4	1220.2
98				3.4	1219.2
T.P.	10.41	1229	73	3.30	1219.32
99				11.1	1218.6
+10	℄ 10" C.I.P. fair			11.1	1218.6



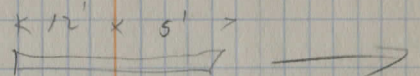




					(CALC. '79)
		1229	73		
100				10.6	1219.1
101				9.7	1220.0
102				8.5	1221.2
103				6.6	1223.1
104				4.3	1225.4
105				1.7	1228.0
T.P.	9.40	1238	84	0.29	1229.44
106				7.3	1231.5
107				4.3	1234.5
108				4.1	1238.7
109				6.2	1232.6
110	& 10 C-1 P.			6.7	1232.1
111				6.7	1232.1
112				6.0	1232.8
113				4.1	1234.7
114				0.5	1238.3
T.P.	5.99	1243	76	1.07	1237.77
+60				2.2	1241.6
115				3.2	1240.6
+50				5.8	1238.0
116				8.6	1235.2
117				13.5	1230.3
T.P.	0.71	1231	67	12.80	1230.96
118				4.8	1226.9
119				7.6	1224.1
120				9.6	1222.1

(Ext.)

× 12' × 5' ×



				(calc. '79)	
		1231	67		
121				12.6	1219.1
T.F.	0.70	1219	64	12.73	1218.94
122				4.5	1215.1
123				6.5	1213.1
B.M.				7.94	1211.70
124				7.7	1218.9
125				8.6	1211.0
1+75	℄ 1½ x ½ stone Box			9.3	1210.3
T.P.	10.37	1221	42	8.59	1211.05
126				10.9	1210.5
+50				10.7	1210.7
127				9.5	1211.9
128				5.1	1216.3
+60				3.0	1218.4
129				4.1	1217.3
130				6.8	1214.6
131				9.2	1212.2
132				10.3	1211.1
+70				10.6	1210.8
133				12.0	1209.4
T.P	0.85	1210	46	11.81	1209.61
134				7.3	1203.2
135				10.5	1200.0
+82	℄ 1½ x 1½	stone Box		11.1	1199.4
136				10.8	1199.9

Spike in N.W. root 30" Elm 30' Rt. Sta 123+75

+75 fair

<8½ 11'>

fair

<9' x11'>

(CALC. '79)

1210 46

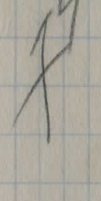
+65			10.6	1209.9
137			9.2	1201.3
138			3.0	1207.5
+25			2.2	1208.3
138+88			3.9	1206.6
+96			3.6	1206.9
T.P.	10.14	1217 65	3.95	1207.51
T.P.	12.43	1228.29	1.79	1215.86
B.M.			1.73	1226.56

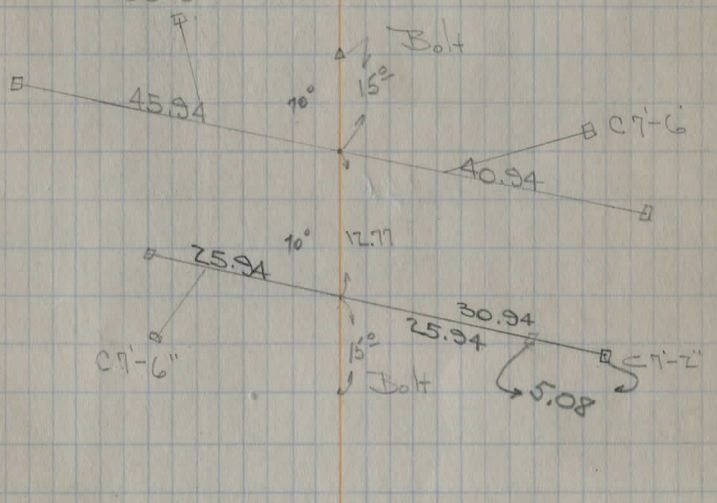
℄ 33" ←".

root "Walnut front of old Zethmayr place

BROWN'S ROAD BRIDGE
No 32-E-10

X on S.E. Cor. Rt wing of S. Abut.





Stakes checked for line & dist. 5/20/39
Pomeroy-Chase-Willman

See next page for levels

Test hole #1 (Near Rt. Cor.)

B.M.	A.C.4	1173.42		1160.70
Ground	Sandy loam		8.37	1165.05
			+2.75	-2.75
End Sandy loam - Begin sandy clay			11.12	1162.30
				-4.50
End " clay. " gravel				1160.55
				-5.20
Begin blue clay				1159.85
" "				7.00
				1158.05

Hole #2 Far Right Cor

1173.42

Ground - Sandy clay	9.94	1163.48
Gravely clay	+1.2	1162.28
Sandy clay	+3.0	1160.48
Unable to sink ½" Rod more than 1½"	+6.0	1157.48

Hole #3 Near left

Ground - Sand Clay	1173.42	9.50	1163.92
Gravely clay		+2.00	1161.92
" " Unable to sink ½" Rod		+6.50	1157.42

Hole #4 Far left

Ground - Gravely clay	1173.42	10.10	1163.32
Gravel Unable to penetrate		+5.0	1158.32

5/20/39 Fair - Warm 65°

Pomeroy & Co.

Check levels Brown Rd. Bridge

	+	H.I.	−	Elev	Grade
B.M.	4.98	1173.76		1168.78	
Replacement B.M.			7.26	1166.50	
Bottom channel			11.76	1162.00	Bot. footings
Far ℄ hub			7.76	1166.00	1158.50
Near ℄ "			8.10	1165.66	"
" Lt "			7.76	1166.00	"
Far " "			8.76	1165.00	"
B.M.	4.76	1171.26		1166.50	
			2.51	68.75	Top slab
			3.55	67.71	

1158.50 = Bot. Footings
2.5
1161.00 = Bot. Wall
6.71
1167.71 = Bot. slab at ℄
1.04
1168.75 = Top slab at ℄

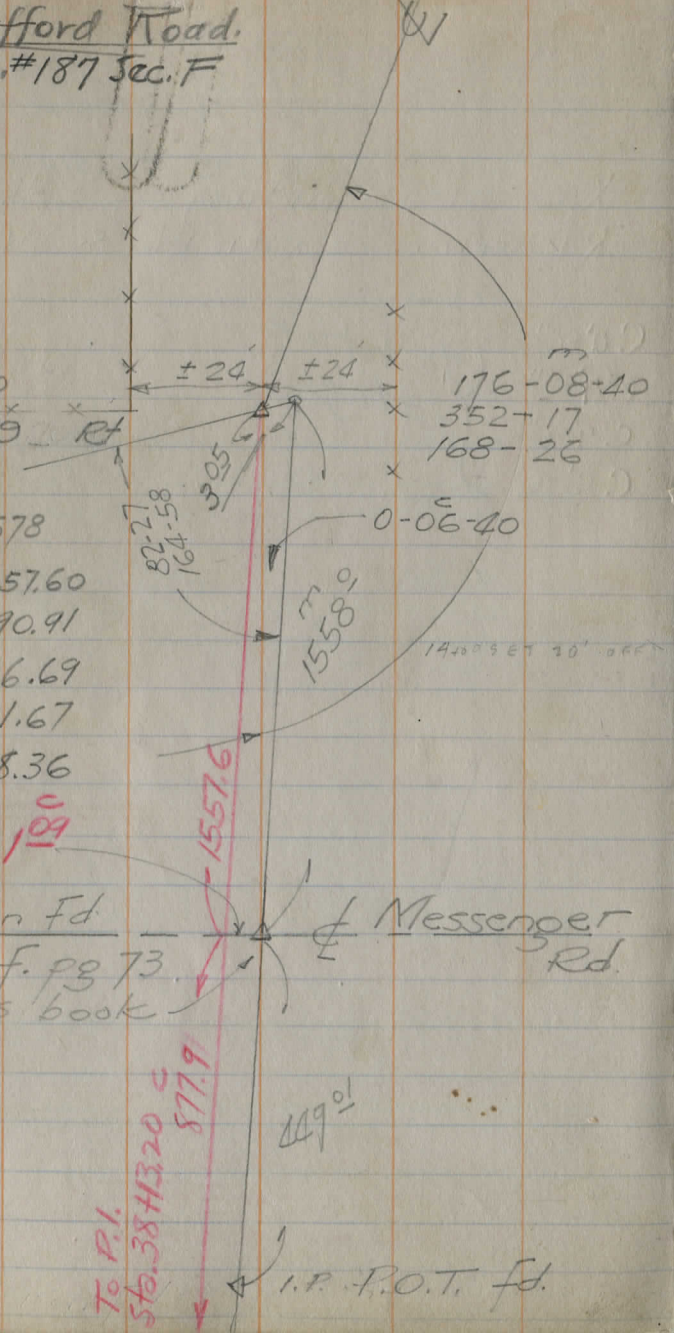
X on S.E. cor. Rt wing of S. Abutt.

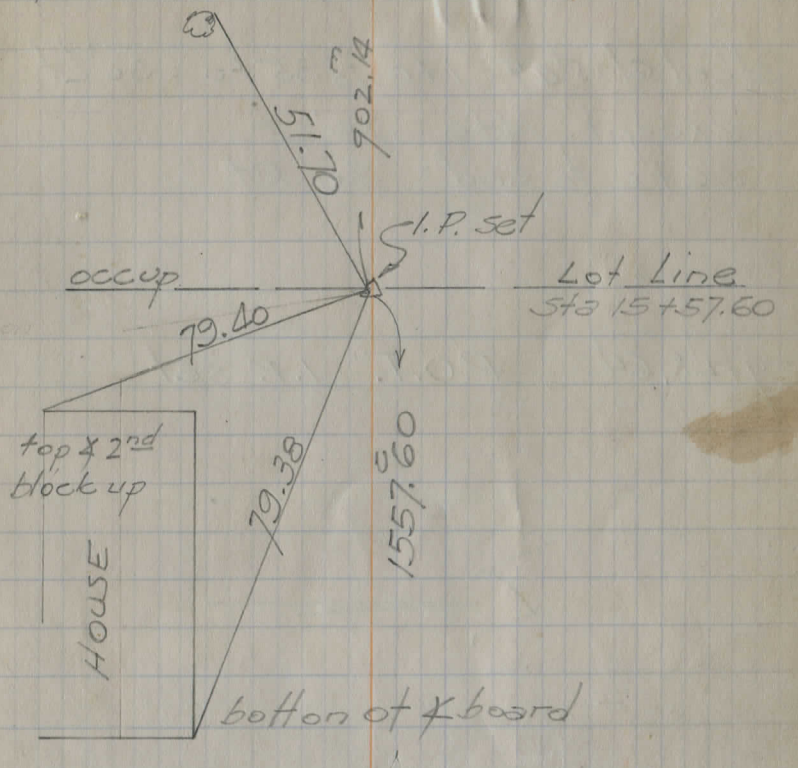
R.P. Set W in S.E. Root 12" Elm 50' S.W. of ℄ Bridge

C 7'-6" } to bottom
C 7'-7" } footings
C 7'-6" }
C 6'-6" }

	65.66	68.78
	7.17	10.00
	58.49	58.78
	10.25	2.50
	68.74	56.28

Stafford Road.
C.H. #187 Sec. F
July '48

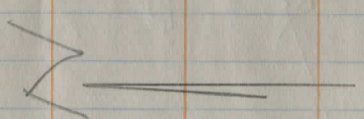




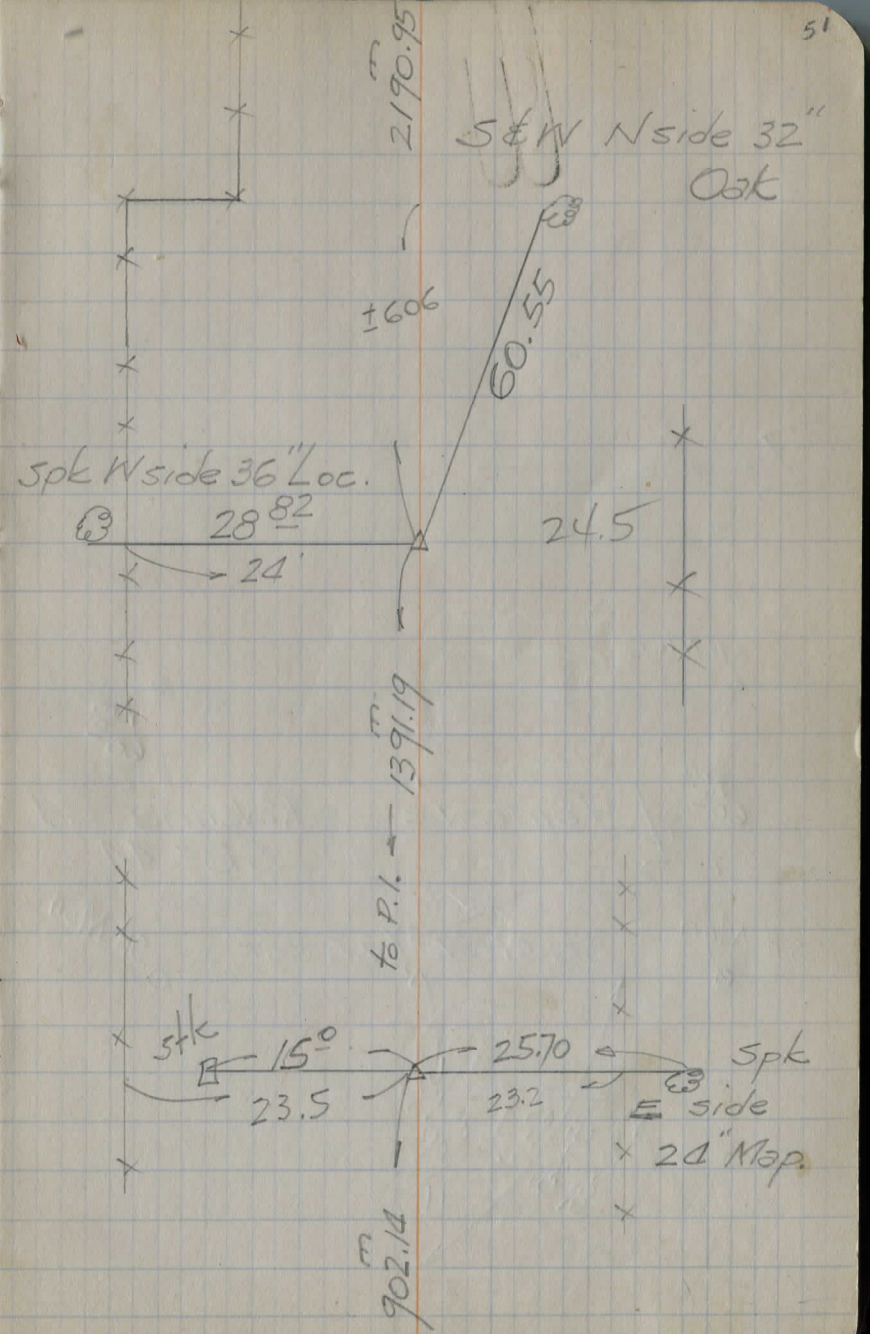
STAFFORD RD
No 187 Sec. F
7-21-48
Maynard
Temple
Pom

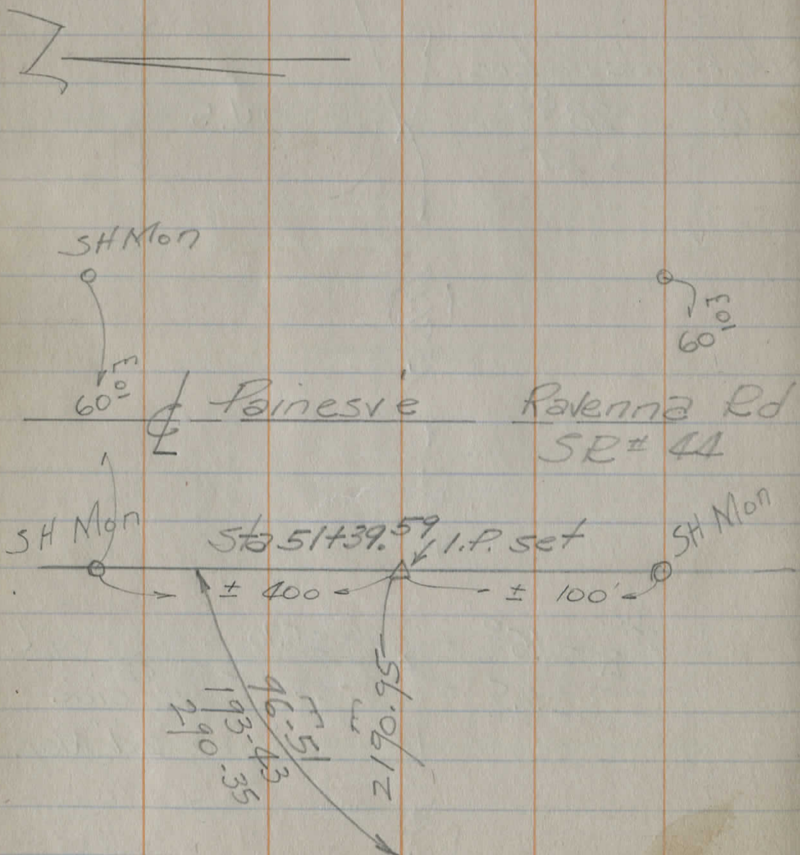
stked 6/25/09. 1+00 to 35+00 = 30' Lt
except 12+00 = 20' Lt
36+00 to end = 30' Rt

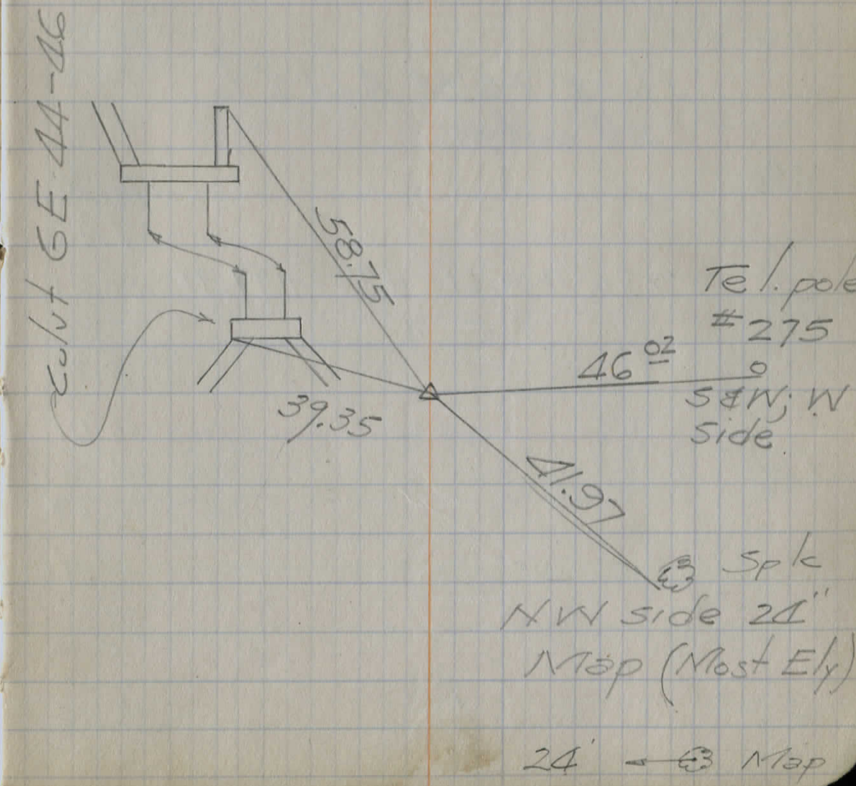
29+48.64 P.O.T. I.P. set



21+59.59 P.O.T. R.R. spike set




SH Mon
60
Painesv'e Ravenna Rd
SR # 44
SH Mon
Sta 51+39.59 I.P. set
SH Mon
± 400
± 100'
60 10.3
2190.95
96.51
193.43
290.35


Cult GE 44-46
58.75
39.35
41.97
Tel. pole
275
46.02
S & W; W side
Spk
NW side 24"
Map (Most Ely)
24' ← Map

STAFFORD ROAD TH #187 E

Final grades for Culvert outlet Sta. 32 +57

1-5-54

B.M.	4.24	1202.85		1198.61	
B.M. set			5.09	1197.76	
					02.85
0+50	NOTE: Stks set on 15' offset both side of ℄ of channel				95.03
					7.82
					02.85
1+0					94.97
					7.88
	NOTE: 1-6-54 Add 2" to all cuts				
					2.85
+50					94.90
					7.96
T.P.	2.70	1200.61	4.94	1197.91	00.61
2+0					94.83
					5.78
					00.61
+50					94.76
					5.85
					00.61
3					94.70
					5.91
					00.61
4					94.56
					6.05

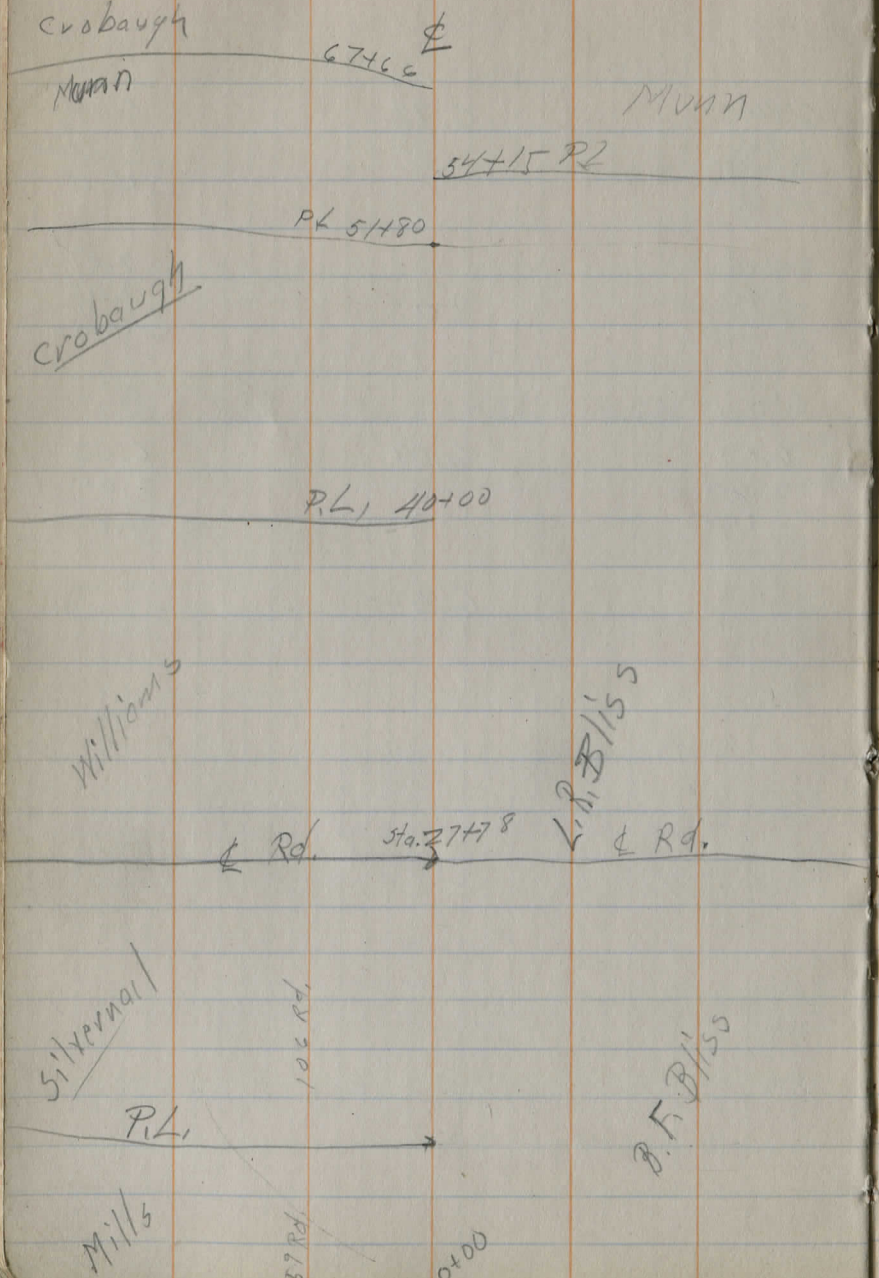
HW ≠ N Hdwl.

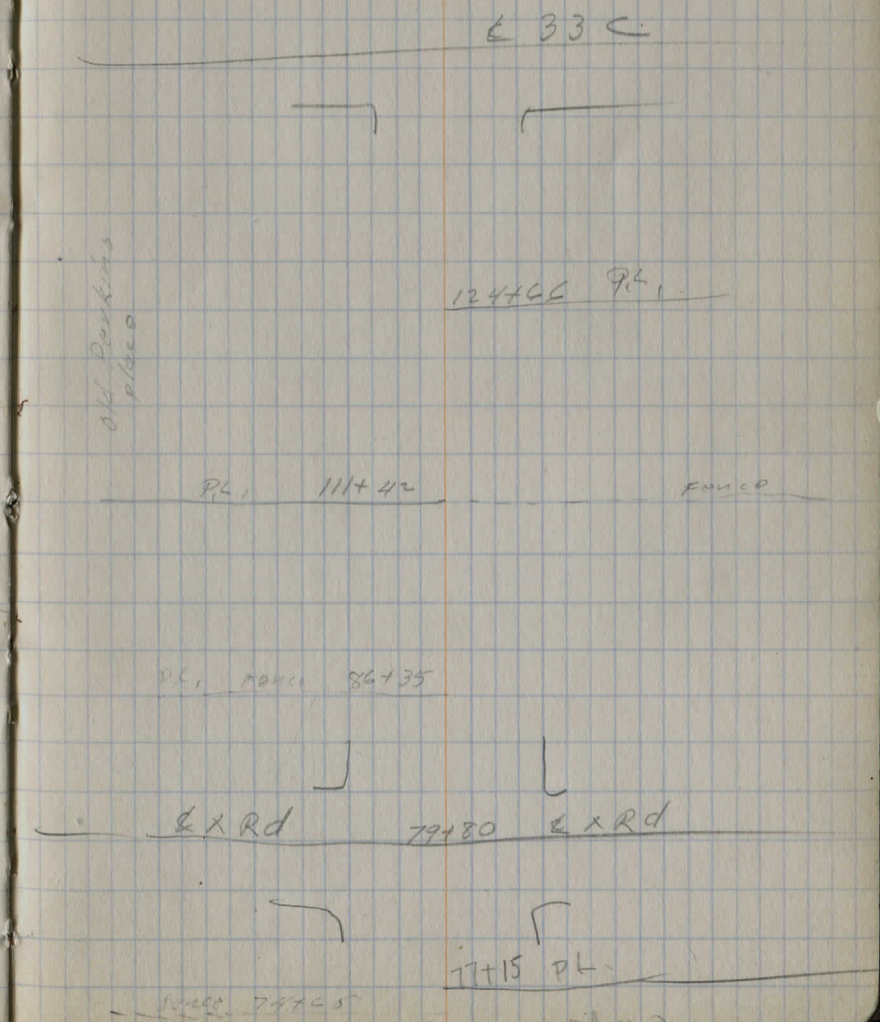
Spk S root 12" Elm ± 60' SE of culv ℄

E	℄ channel	W
7.82	7.59	4.34 r
4.32 r		C 3.5
C 3.50		
7.88	7.51	7.88
4.88 r		4.90 r
C 3.0		C 3.0
7.95	7.58	7.95
4.93 r		4.94 r
C 3.0		C 3.0
5.78	5.32	12 5.78
2.78 r		2.78 r
C 3.0		C 3.0
5.85	5.42	5.85
2.35 r		2.35 r
C 3.5		C 3.5
5.91	5.57	5.91
2.94 r		2.91
C 3.0		C 3.0
3.05 r	5.76	6.05
C 3.0		3.05 r
		C 3.0

		1200.61				East		West	
T.P.	3.82	1201.37	3.06	1197.55					
					01.37	6.94		6.94	
5					94.43	2.94	6.72	2.94	
					6.94	C4.0		C4.0	
					01.37	7.07		7.07	
6					94.30	3.00	7.0	3.05	
				(96.80	7.07	C4.0		C4.00	
T.P.	3.35	00.19	4.53	96.84	00.19	Hob C			
7					94.16	6.03	6.09	6.03	
					6.03	2.03		2.04	
					00.19	C4.0		C4.0	
8					94.02		6.32		
					6.17				

PROPERTY LINES





74465

MAGNETIC SPRING ROAD C.H. #4

Sta.

10

9

8

7

6

5

4

3

N.4°-45' E.

2

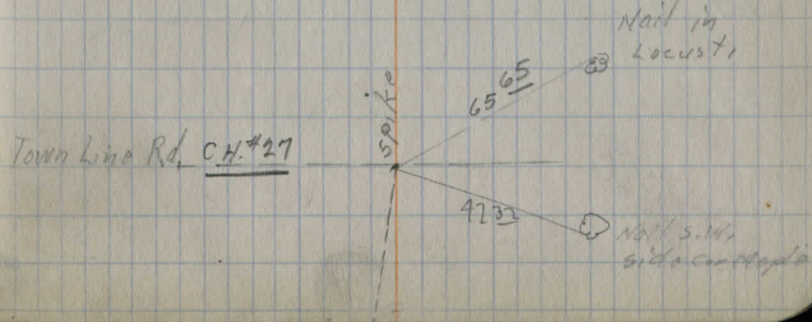
1

0

9-17-'24

Hanna
Sprague
Douglass

℄



Sta

22

+35.1 Δ 0°-0'

21

20

19

18

17

16

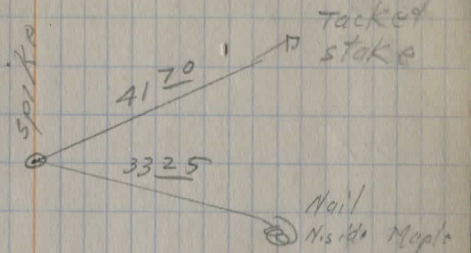
15

14

13

12

11



Sta.
35
34
33
32
31
30
29
28
27
26
25
24
23

+41.4 Δ

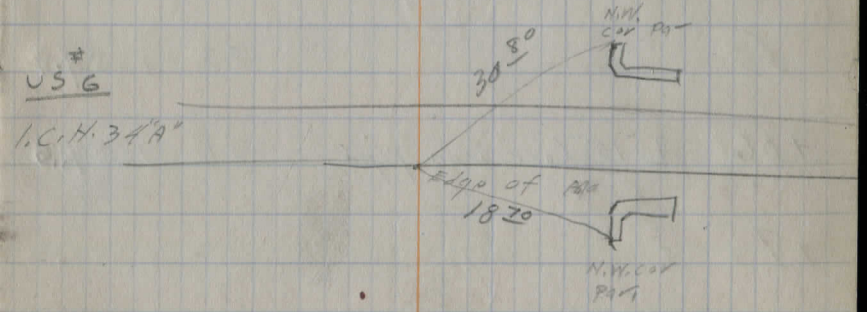
38

37

36

USG

I.C.H. 34A"



Magnetic Spring Rd. X Sections
C.H. #4

9-17-'24 PM
cloudy
Hanna
Sprague
Douglass

61

	B.S.	H.I.	F.S.	Elev.	
~~B.M.~~	~~B.S.~~				
B.M.	4.90			1256.17	S.W. Cor. Stone door step School House GONE
0			6.1	1255.0	
+22	E 12" C.I.P.		4.1	1255.0	
1			5.2	1255.9	
2			4.1	1257.0	
3			3.4	1257.7	
4		1261.07	3.8	1257.3	
T.P.	4.97		3.31	1257.96	
5			5.8	1256.9	
6			5.3	1257.4	
+06	E 15" Corr Iron pipe		5.1	1257.6	
7			4.4	1258.1	

7.7/25 6.1 4.8/25

8.4/25 8.0/7.5 6.6/7 6.1 5.5/5 5.3/19 7.7/19.5 6.9/25

7½ × 18

5.5/20 5.3/13 5.4/10 5.2/6 4.8/7.7 4.6/13 3.7/20

4.9/20 4.5/12 3.8/3 4.1 4.3/7 4.4/8 3.4/14 2.2/20

4.0/20 3.8/14 4.0/12 3.2/3 3.4 4.0/10 2.7/13 2.9/20

4.0/20 4.1/12 3.4/2 3.8 4.1/10 3.7/14 3.0/17-20

6.6/20 6.0/15 6.5/12 4.1/7 5.5/2 5.8 6.2/7 6.0/8 6.7/9 5.7/14 5.3/26

5.5/20 4.9/10 5.0/6 5.7 5.2/8 7.0/10-11 5.1/14 5.0/20

9.5/130 8.3/100 7.3/50 7.5/7.4 6.2/10 5.1/6 5.1 5.2/8 5.8/11 7.1/7.4 5.0/16-20

← 10' × 11½ →

4.8/20 4.5/14 4.9/12 4.3/4 4.6 4.6/5 4.8/7 4.3/9 3.9/15 3.8/20

8			3,8	1258.9
9			3.9	1258.8
10		1262.73	4.4	1258.3
T.P.	2.16		3.48	1259.25
11			4.0	1257.4
12			5.3	1256.1
+26	@ 12" C.I.P.		5.2	1256.2
13			5.4	1256.0
14			4.7	1257.2
15			4.9	1256.5
16			6.9	1254.5
17			6.2	1255.2

1261.0

$\frac{43}{20}$ $\frac{40}{16}$ $\frac{47}{14}$ $\frac{33}{4}$ $\frac{38}{}$ $\frac{37}{6}$ $\frac{40}{7}$ $\frac{30}{10}$ $\frac{25}{20}$

$\frac{46}{20}$ $\frac{43}{16}$ $\frac{47}{15}$ $\frac{44}{12}$ $\frac{37}{3}$ $\frac{39}{}$ $\frac{40}{5}$ $\frac{43}{8}$ $\frac{30}{12}$ $\frac{32}{15}$ $\frac{30}{20}$

$\frac{47}{20-18}$ $\frac{44}{13}$ $\frac{48}{11}$ $\frac{40}{2}$ $\frac{44}{}$ $\frac{47}{6-8}$ $\frac{36}{11-20}$

$\frac{42}{20-12}$ $\frac{47}{10}$ $\frac{41}{1}$ $\frac{40}{}$ $\frac{44}{9}$ $\frac{48}{10}$ $\frac{30}{14}$ $\frac{31}{17-20}$

$\frac{60}{20}$ $\frac{55}{10}$ $\frac{58}{8}$ 5.3 $\frac{54}{11}$ $\frac{59}{13}$ $\frac{49}{15}$ $\frac{50}{20}$

$\frac{98}{100}$ $\frac{83}{50}$ $\frac{77}{12}$ $\frac{79}{54.9}$ $\frac{65}{8}$ $\frac{60}{6}$ $\frac{52}{}$ $\frac{56}{8-10}$ $\frac{74}{11}$ $\frac{72}{15}$

<8 × 10½

$\frac{55}{20-11}$ $\frac{60}{8}$ $\frac{54}{}$ $\frac{52}{2}$ $\frac{57}{11}$ $\frac{59}{12}$ $\frac{48}{20}$

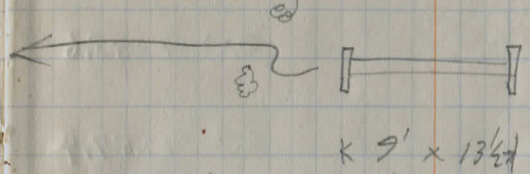
$\frac{51}{20}$ $\frac{52}{8}$ $\frac{42}{}$ $\frac{40}{1}$ $\frac{48}{11}$ $\frac{52}{12}$ $\frac{46}{13}$ $\frac{41}{20}$

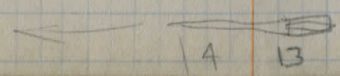
$\frac{51}{20}$ $\frac{54}{12}$ $\frac{61}{9}$ $\frac{49}{}$ $\frac{59}{11}$ $\frac{46}{14}$ $\frac{40}{20}$

$\frac{69}{20}$ $\frac{79}{14}$ $\frac{77}{11}$ $\frac{69}{70}$ $\frac{69}{1}$ $\frac{74}{11}$ $\frac{78}{14}$ $\frac{66}{20}$

$\frac{80}{20}$ $\frac{88}{14}$ $\frac{61}{1}$ 6.2 $\frac{59}{9}$ $\frac{85}{14-20}$

17+08 ℄ 3×3 Stone Box			5.8	1255.6	10.1/F.L. 9½ 4.5/Par 5.8 4.5/Par 10.1/F.L. 14
		↑			
		1261.41			
T.P.	5.71		4.49	1256.92	S.W. Cor ~~W.~~ H. Wall
18			8.3	1254.3	20-12/9.8 8/9.6 4/9.1 8.3 4/8.4 8/8.3 16/9.3 20/9.4
19			8.0	1254.6	20-8/8.6 4/8.4 8.0 2/7.7 6/8.1 10/8.2 12-20/8.7
20			6.2	1256.4	20/5.2 16/5.5 8/6.1 6/6.7 4/6.5 6.2 3/5.8 15-20/6.9
21			3.4	1259.2	20-10/3.5 9/4.0 3.4 2/3.0 15/4.7 18-20/3.1
22			3.1	1259.5	20/3.3 10/3.5 8/3.4 3.1 3/2.9 13/3.2 15/3.5 17-20/3.0
23			3.2	1259.4	20/4.2 12/3.8 8/3.9 7/3.6 3.2 3/2.6 14/3.4 16/2.7 20/2.2
		↑			
24		1262.63	4.0	1258.6	20-14/4.5 8/4.8 5/4.3 4.0 4/3.6 14/4.5 17-20/3.7
T.P.	2.62		1.70	1260.93	
25			5.2	1258.4	20-11/5.7 10/5.8 8/5.6 5.2 4/4.8 13/5.2 15/5.6 16-20/5.1
24+13 ℄ 8" C.I.P. & V.P.			5.1	1258.5	50/7.5 30/7.0 8/6.5 6/5.7 5.1 4/4.8 12/5.2 13/5.6 F.L. 14/6.2





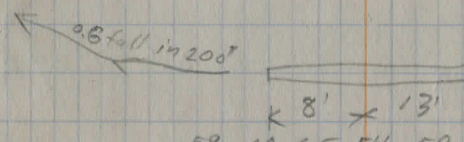
26			3.5	1260.1
27			5.0	1258.6
28			6.2	1257.4
29			6.4	1257.2
+03 ℄ 14" C.I.P.				
30			5.4	1258.2
9-18-'24 Fa... Warm		1263.55		
T.P.	3.91		1.88	1261.67
31			5.8	1259.3
+13 ℄ 3½ × 2½ Stone Box			5.2	1259.9
32			5.4	1259.5
33			4.6	1260.5

3.8/20 4.0/10 4.3/8 3.5 3.2/1 4.2/13 3.3/15 3.0/20

20 4.9/15. 5.1/10. 5.8/7. 5.0 5.6/9. 6.2/11. 4.6/16. 3.8/20.

5.6/20 5.9/10 6.5/7 6.6/6. 6.2 6.0/2. 6.6/11. 7.1/12. 6.0/15-20.

8.6/200 8.2/125 8.2/75 8.0/20 6.8/16 8.0/FL. 3½ 6.7/8 6.6/4 6.4 6.1/4 5.8/12 6.5/13 7.7/13½ FL. 7.4/16

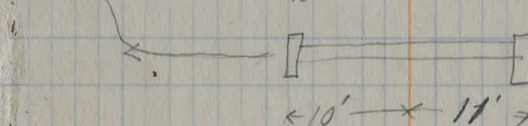


20 5.9/14 6.0/9 6.5/8 5.4 5.0/3 5.3/8-12 5.8/16 4.6/20

S.E. Cor. W. Head Wall

20 6.8/17 7.1/13 6.0/7 5.8 5.8/8 6.6/15. 6.2/20

10.6/250 8.5/100 8.2/18 8.5/FL. 10½ 3.9/9ar 5.7 4.0/9ar 8.5/FL. 11½



20-18 6.1 5.4/13 6.3/12 5.4/2 5.6 5.9/5 5.3/6 6.3/12 5.7/15-20

20 4.9/13 5.5/12 5.3/7 4.6/3 4.6 4.4/5 4.0/6 5.1/12 4.5/14. 4.3/20

		↑		
34		1265.08	2.6	1262.5
T.P.	11.89		0.68	1264.40
35			9.1	1267.2
36			6.4	1269.9
37			5.8	1270.50
38			3.6	1272.7
		↑		
+414		1276.29	1.1	1275.19
T.P.	4.29	1274.56	6.02	1270.27
B.M.			11.73	1262.83

$\frac{32}{20}$ $\frac{31}{12}$ $\frac{34}{10}$ $\frac{32}{6}$ $\frac{26}{2}$ $\frac{24}{7}$ $\frac{25}{10}$ $\frac{34}{15}$ $\frac{25}{16}$ $\frac{23}{20}$

$\frac{69}{20}$ $\frac{71}{18}$ $\frac{76}{14}$ $\frac{97}{12}$ $\frac{91}{8}$ $\frac{91}{1}$ $\frac{90}{1}$ $\frac{97}{5}$ $\frac{115}{15}$ $\frac{103}{17}$ $\frac{91}{20}$

$\frac{68}{20}$ $\frac{69}{13}$ $\frac{74}{11}$ $\frac{64}{9}$ $\frac{67}{9}$ $\frac{80}{15}$ $\frac{64}{18-20}$

$\frac{61}{20-15}$ $\frac{62}{9}$ $\frac{58}{7}$ $\frac{56}{7}$ $\frac{62}{15}$ $\frac{51}{17-20}$

$\frac{36}{20-14}$ $\frac{42}{10}$ $\frac{36}{15}$ $\frac{37}{15}$ $\frac{47}{17}$ $\frac{35}{20}$

End = edge of Pavement

S. root Sycamore 400' W. on N. side Park

Feb. 2, 1931, Fair, 35°

Marks, Parks, Snyder, Merritt

36+00	0°00'	Iron Pin Top of Hill
32+00		Foot of Hill
20+00	0°00'	Spike on ℄
19+44.3		Bridge, Steel Beams " Railings.
10+00	0°00'	Spike on ℄
6+00	0°00'	Stake on ℄, Summit.

0+00, Stafford Rd. = 78+45.5, Brown's Cor. Rd.

STAFFORD ROAD, SEC. B. 66
AUBURN TWP.
T.H. 187

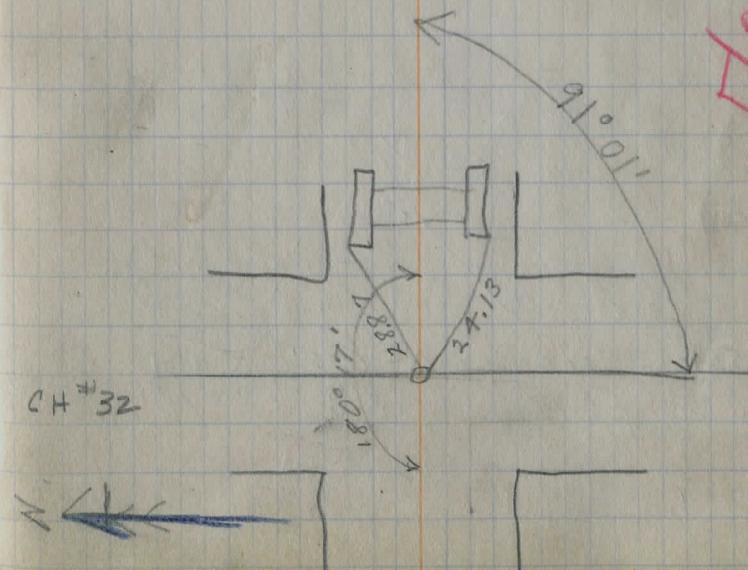
22'

Mag. S86°E

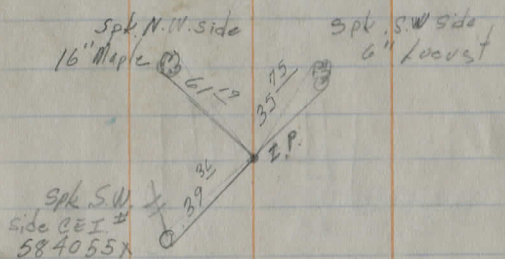
Staked on Offset of 20' Right at every 200' (Even Numbered stations)

Now SEC. C-D

Span, 16' Abut to Abut. 4.1 9.9
Rail Length.

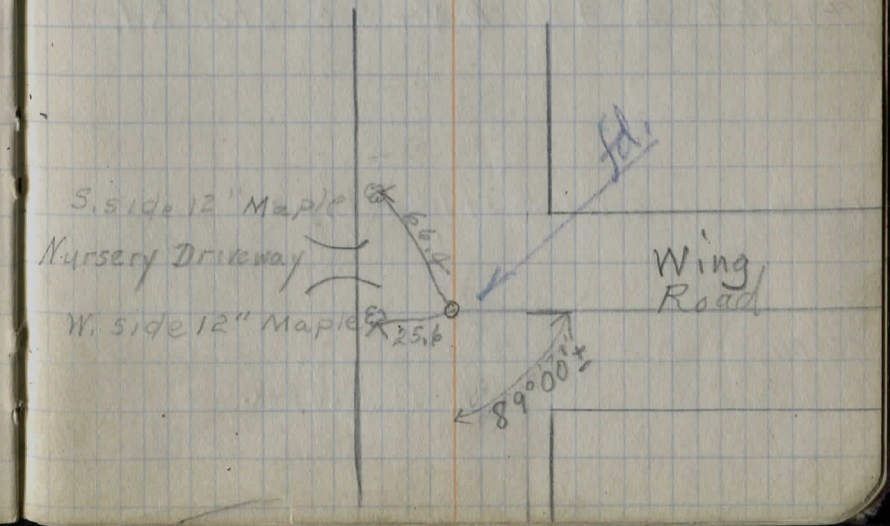


45+97.14 Δ = 0°00' Iron Pin



36+95.54 Iron Pipe Δ = 0°16' Right
Fd. 10/8/64 & replaced w/ ½" x 14" I.P.
10" in Ref. above

Ditch
59+00
12.0' 6.5'
58+59
12" Solid Cast Iron Pipe
House
6" Pine tree
26.92
49.92
fd 2"
Fd 10/4/64
Barn
45+97.14
M.Ik House
20.25
Iron Pin
Barn
21.3



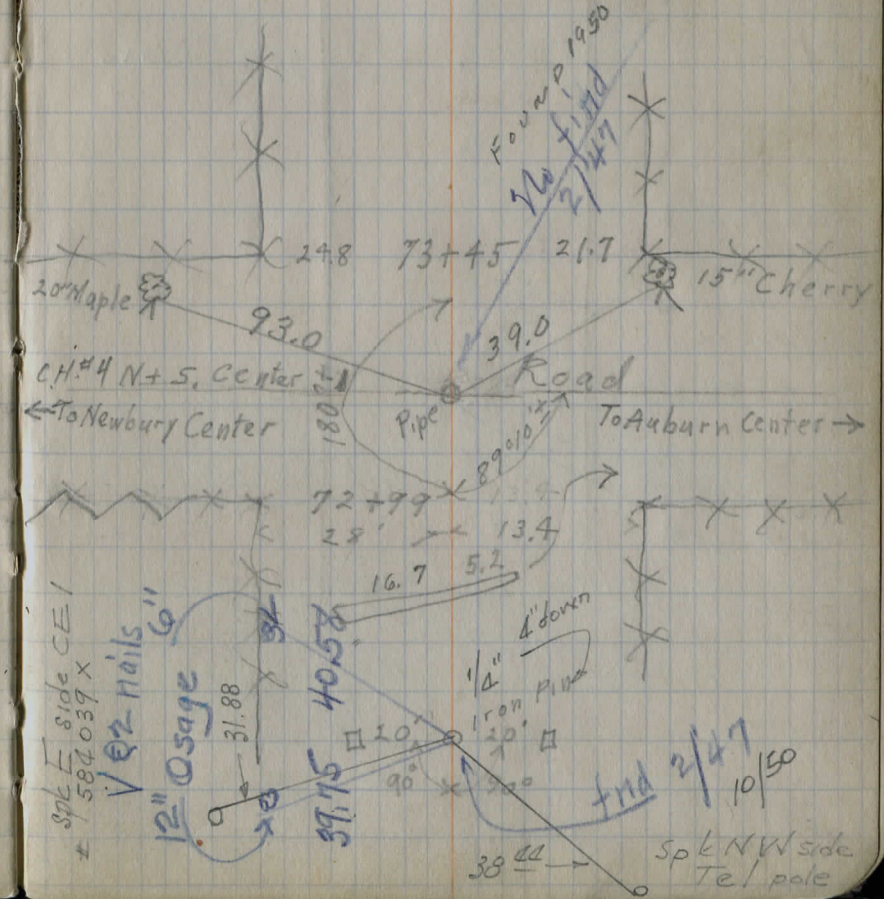
1.387 miles

73+24.4 ℄ Auburn N.+S. Center Rd.

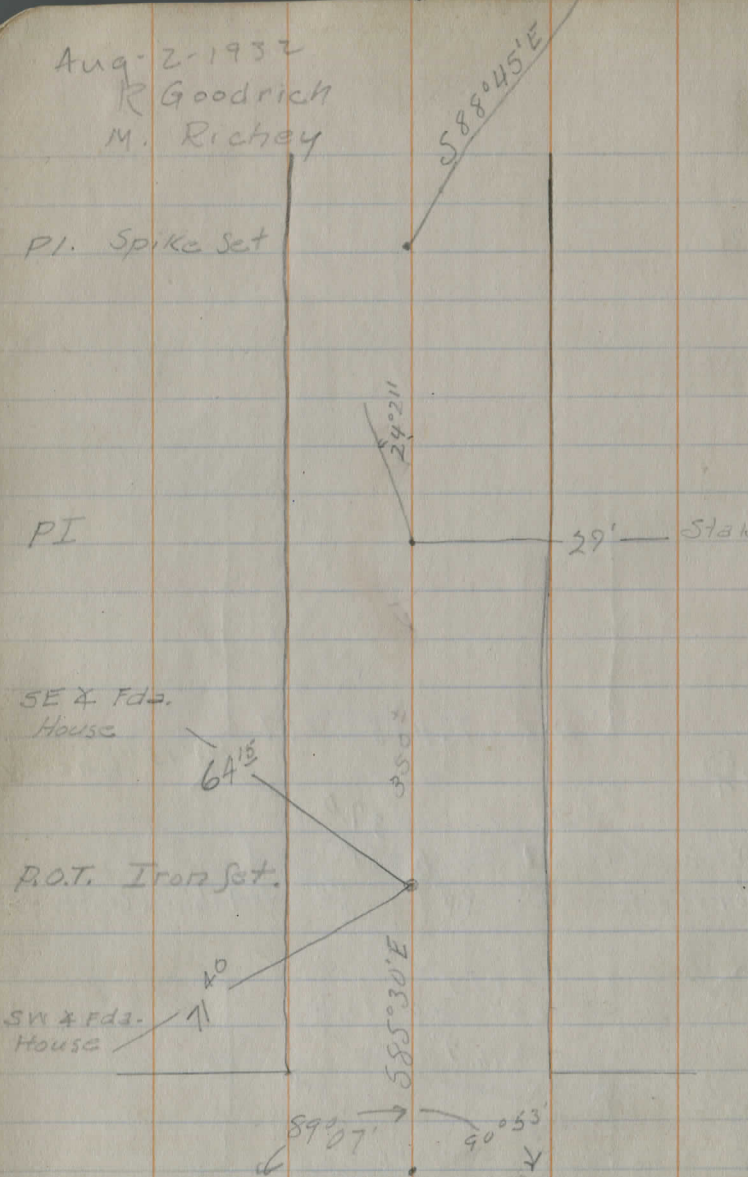
72+76.9 10" Solid Cast Iron Pipe

66+00 Δ = 0°00'

Fd w/ 10/64 50 Ref.



Aug-2-1932
R Goodrich
M. Richey



TH 137

6-17-91 Pomeray
Richards
Gundersen

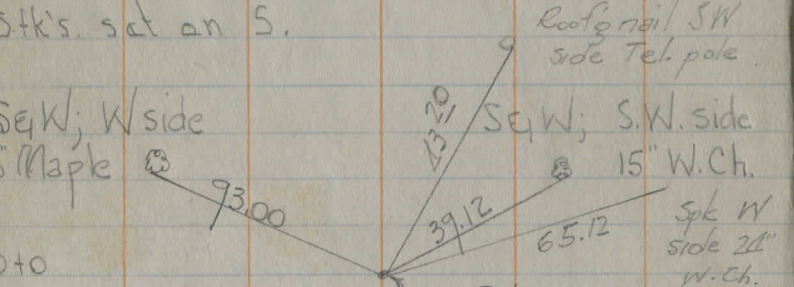
STAFFORD ROAD

16+0 Quit

14+99 4'x2'x20.5' Stone Culvt
North cover stone gone
Culvt fair

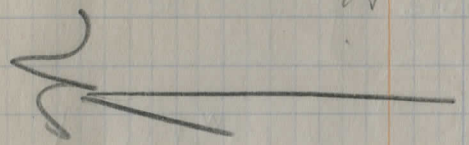
6+02 12"x20' C.I.P. Filled

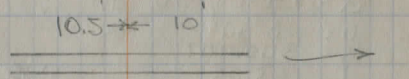
Stk's. set on S.

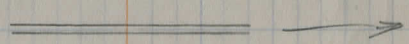


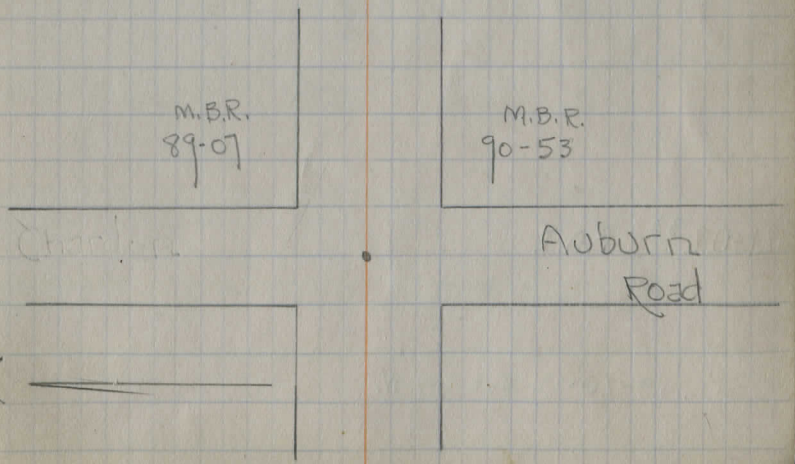
0+0

~~CHARDON~~ AUBURN ROAD EAST
TO Messenger Rd.









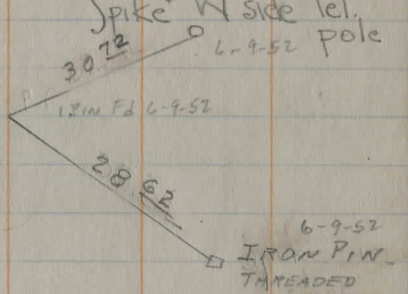
6-19-51
Richards
Gundersen Hot

26+90 12" C.I.P culvt. N.G.
Eliminate if possible

P.T. 25+16.88

24+46.88 Δ = 24°02'-30
D = 18°30'
R = 309.707
T = 65.95
L = 129.95
E = 6.94

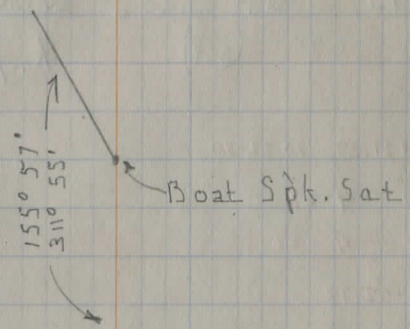
P.C. 23+80.93

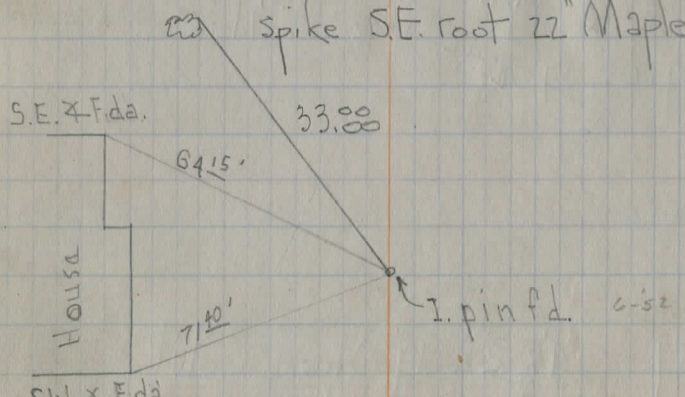


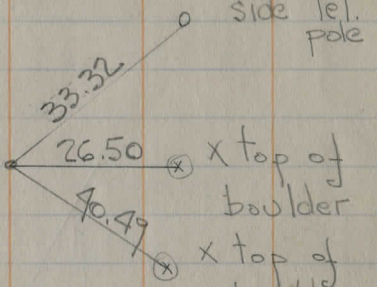
21+02.32 P.O.T.

Stk's. 19-20-21 Sat on N.

16' → swamp







42+39.65 Boat spike (set) F.L. 6-50

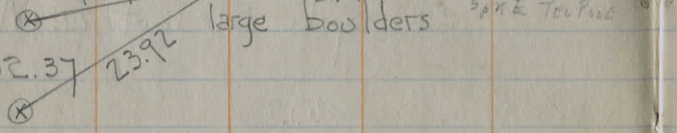
PT 39+21.23 10-22-30

39 9-22

38 40-37

P.C. = 37+02.78

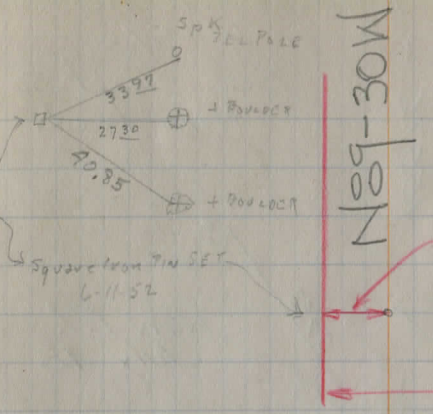
P.T. = 39+21.58



38+13.20 Xs on large boulders

P.C. = 37+02.37

32+57 4'x2'x1' Stone Culvt. Not so good " " " 6-52



Δ = 20-45-10

D = 9-30

R = 603.113

T = 110.42

L = 218.45

E =

Δ = 20°-49'-30" Rt

D = 9°-30'

R = 603.113

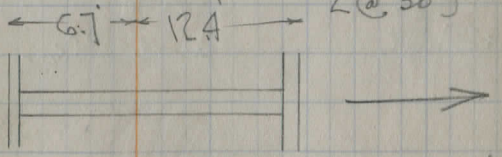
T = 110.83

L = 219.21

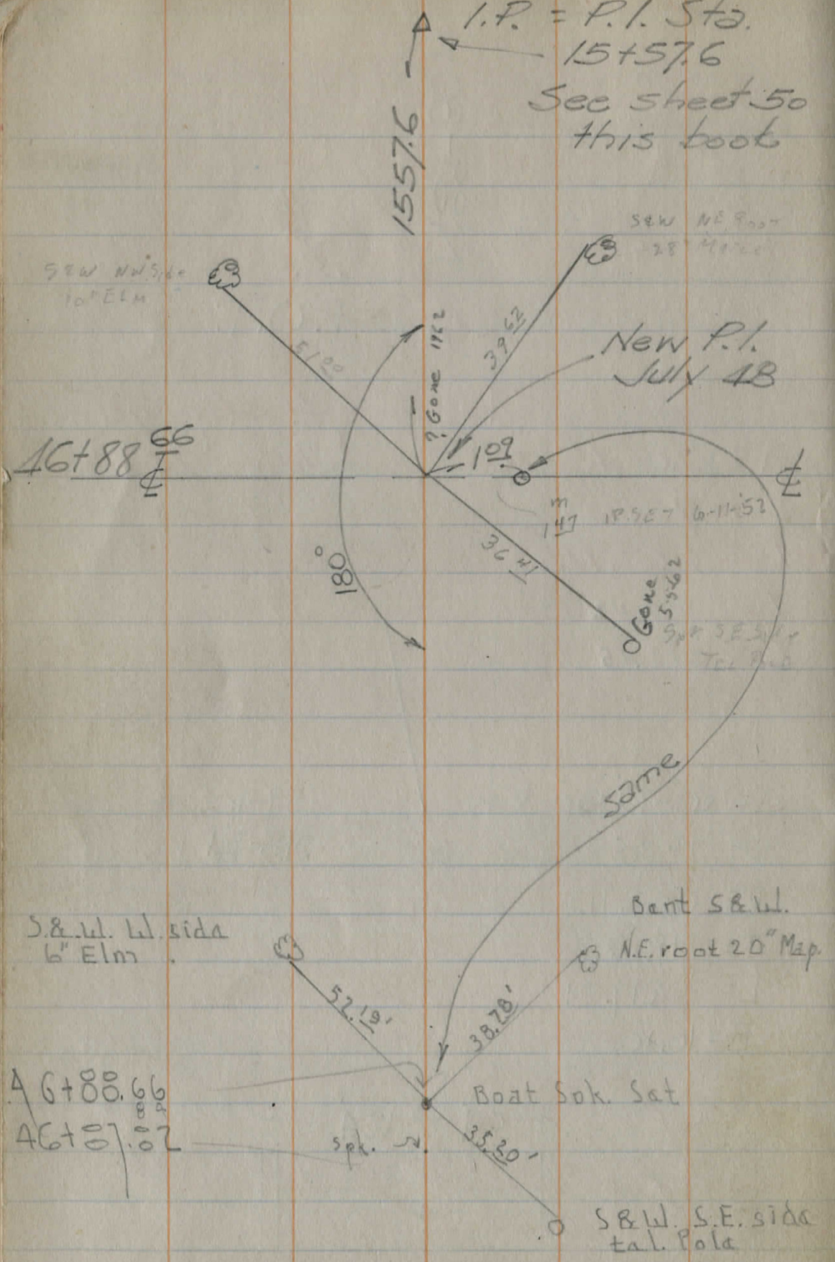
E = 10.10

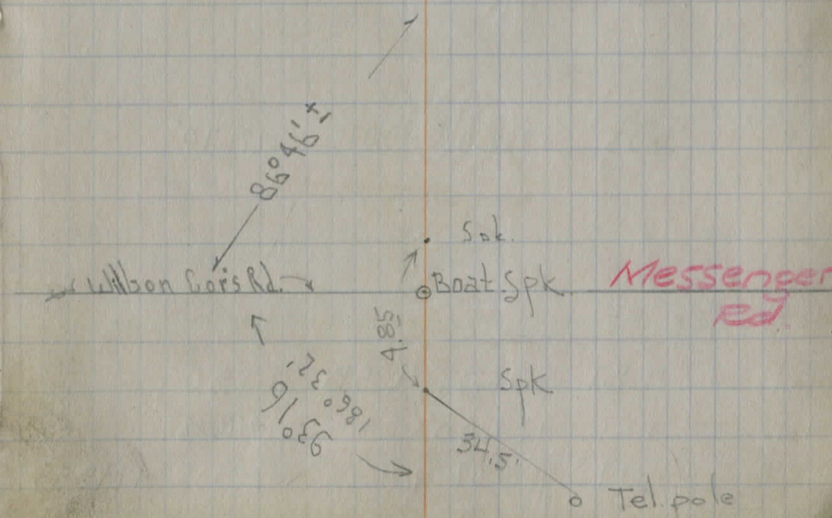
159-10

318-21



See pg 27 this book for outlet levels Dec '53


I.P. = P.I. Sta.
15+57.6
See sheet 50
this book
1557.6
39.62
New P.I.
July 48
46+88 66
109
147
I.P. SET 6-11-52
36.41
180°
Gone
Same
Bent S&W.
N.E. root 20" Map.
S.&W. W. side
6" Elm
52.19'
38.78'
46+88.66
46+87.02
Boat Spk. Set
spk.
35.30'
S&W. S.E. side
tel. Pole


86°46'
Wilson Cors Rd.
Spk.
Boat Spk
Messenger Rd
4.85
93°16'
186°32'
Spk
54.5'
Tel. pole

	+	H.I.	−	E		
32					97.37	4.4
B.M.#4			3.16	1198.61		x N.W. & N. Hdwl Culvt. sta 32+57
33					98.27	3.5
T.P.	2.76	1201.27	11.14	1199.01		
34					99.05	11.1
35					00.95	9.2
36					02.65	7.5
37					04.45	5.7
B.M.#5	1.89	1210.15	3.10	1208.26		x on 2nd boulder W. of P.I. N. side rd.
38					07.14	4.2
T.P.	0.92	1211.36	11.59	1210.44		
39					10.03	R.0
40					14.63	7.4
41					18.73	3.3
42					21.33	0.7
43					21.73	0.3
T.P.	0.33	1222.03	3.07	1221.70		
44					21.57	3.2
45					21.57	3.2
46					20.77	4.0
+88.66					18.57	100'S 8.2 Wilson Cor's 6.2 Sta. 100' N 2.7
T.P.	12.87	1224.77	0.58	1211.90		100'E 6.3
T.P.	1.66	1212.48	9.80	1210.82		
B.M.	1.07	1220.62			1219.55	S. root 36" Pine Lt Sta 76+68 Wilson Cor's N. rd.

	+	H.I	-	E		S		N
14					99.21		6.4	
Culvt.					99.21	← ? F.L. 12.3 93.31	6.4	F.L. 12.5 1193.11
15					1199.11		6.5	
16					1200.61		5.6	
B.M. #3			2.51	1203.10		Spk. S root 28" Map 25' Lt. Sta 17+10 (Lt. and tree row)		
17					1201.81		3.8	
T.P.	1.97	1205.61	8.59	1203.64				
18					04.33		7.9	
19					06.13		6.1	
20					07.13		5.1	
21+0					09.13		3.1	
21+10					09.23	Summit	3.0	
22					04.13		8.1	
23					02.63		9.6	
24					1201.63		10.6	
T.P.	10.65	1212.23	0.57	1201.58				
25					99.75		2.4	
26					98.25		3.9	
27					97.65		4.5	
28					98.35		3.8	
T.P.	2.36	1202.15	1.98	1199.79		J.P. on rock rt. Sta 29+10		
29					99.27		2.5	
30					99.17		2.6	
31					97.97		3.8	
		1201.77						

	+	H.I.	−	E		
100' N					10.56	0.5
100' S					04.56	6.5
100' W					09.46	1.6
0+0					08.16	2.9
B.M.# 1			4.62	1206.44		Sp.k. N root 2nd Cherry S of Stafford Rd + E of Ctr. rd.
1					06.56	4.5
2					05.26	5.8
3					03.96	7.1
4					02.76	8.3
5					1200.06	11.0
T.P.	11.63	1211.06	8.61	1199.43		
6					99.3	8.7
7					99.3	8.7
8					1200.74	7.3
B.M.#2			5.84	1202.20		S root 30" Map. 8+50 15' N. of ℄
9					02.94	8.1
+50					04.19	3.9
10					03.64	4.4
11					03.14	4.9
12					02.04	6.0
T.P.	7.58	1208.04	5.15	1200.46		
13					99.81	5.8
		1205.11				

	+	H.I.	−			
					(1) ↓	
B.M.			0.79	1219.14	1219.55	B.M. on Wilson Cor's. Rd.
T.P.	11.36	1219.93	2.96	1208.57		
T.P.	2.26	1211.53	11.76	1209.27		
T.P.	0.93	1221.03	5.67	1220.10		
T.P.	2.06	1225.77	0.00	1218.71		
B.M.#5			10.97	1207.74	1208.26	
T.P.	11.37	1218.11	0.84	1207.34		
T.P.	9.10	1208.18	3.20	1199.08		
B.M.#4			4.02	1198.26	1198.61	
T.P.	2.82	1201.28	2.99	1199.46	1199.79	rock
T.P.	2.51	1202.45	9.39	1199.94		
T.P.	2.05	1209.33	0.79	1207.28		
BM#3			5.07	1203.00	1203.10	
T.P.	8.05	1208.07	4.88	1200.02		
T.P.	1.77	1204.90	2.75	1203.13		
BM#2			3.66	1203.22	1202.20	
T.P.	6.31	1205.88	10.03	1199.57		
	3.16	1209.60				
B.M.#1				1206.44		

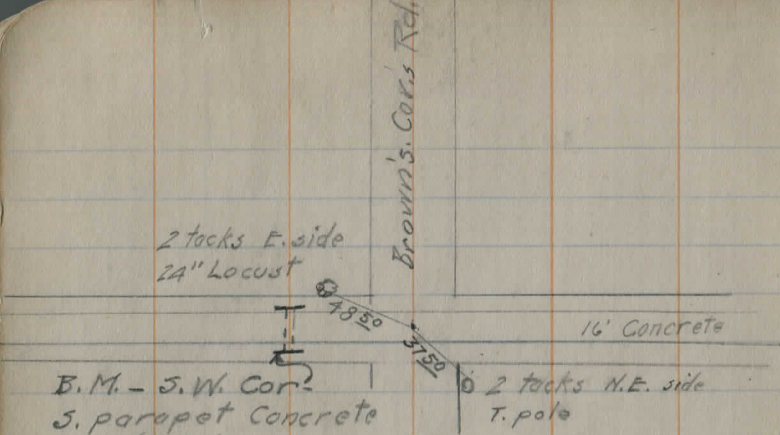
	+	H.I	−		
Grades on ditch N. of Culvt at Sta. 32+57					
600'N					
T.P.	4.38	1201.79	9.48	1197.41	
500'N					
400'N				96.2	
300'N				96.1	
T.P.	9.47	1201.89	5.34	1197.42	
200'N				96.2	
100'N				95.7	
				1195.1	
200'S				1195.5	
100'S				1195.3	
				1195.3	
B.M.#4	4.15	1202.76			1198.61

See pg 77 For outlet levels run 12-53

50'W 4.4 5.0 50'E 4.4

5.4
5.7
5.8

6.6
7.1
F.L.N 1.7
7.3
100'S 5
7.5
F.L.S 5
1.5



B.M. – S.W. Cor.
S. parapet Concrete
Headwall –
Elev. = 1161.81

Main Market Intersection

B.M. #15 on Soules Corners Rd. = C.H. #10
Nail in E. root of 36" Maple
Sta 208 N. side of Rd.
Elev = 1232.41

93+73 Nail N.E.
root of 14" Map.
E. 1227.23

83+73
X on SW Cor.
of E hdwl Cul
1208.99

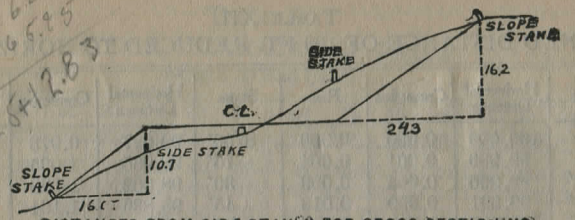
49 45 20
39 + 05 20
10 40.50

IMPROVED TABLES

AND

INFORMATION

Wilber Derrick



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1 65	1 80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3 45	3.60	3 75	3.90	4.05	4.20	4 35	2
3	4.50	4 65	4.80	4.95	5 10	5 25	5 40	5.55	5.70	5.85	3
4	6.00	6 15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7 50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9 00	9 15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10 65	10.80	10.95	11.10	11.25	11.40	11.55	11 70	11.85	7
8	12.00	12 15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13 50	13 65	13 80	13 95	14.10	14.25	14.40	14 55	14.70	14.85	9
10	15.00	15 15	15 30	15 45	15.60	15.75	15.90	16.05	16.20	16 35	10
11	16 50	16 65	16 80	16.95	17 10	17.25	17.40	17.55	17.70	17.85	11
12	18 00	18.15	18.30	18 45	18.60	18 75	18.90	19.05	19.20	19 35	12
13	19 50	19 65	19.80	19.95	20.10	20.25	20 40	20.55	20.70	20.85	13
14	21.00	21 15	21.30	21.45	21 60	21.75	21.90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24 15	24 30	24 45	24.60	24.75	24 90	25 05	25.20	25.35	16
17	25.50	25 65	25.80	25 95	26.10	26 25	26 40	26.55	26.70	26.85	17
18	27.00	27 15	27.30	27 45	27.60	27.75	27.90	28.05	28 20	28.35	18
19	28 50	28 65	28 80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30 00	30 15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31 50	31 65	31.80	31.95	32 10	32 25	32.40	32.55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33.60	33 75	33.90	34.05	34.20	34.35	22
23	34 50	34 65	34.80	34.95	35.10	35 25	35 40	35.55	35.70	35 85	23
24	36.00	36 15	36.30	36 45	36.60	36.75	36.90	37.05	37 20	37.35	24
25	37.50	37.65	37 80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39 00	39 15	39.30	39 45	39 60	39.75	39.90	40.05	40.20	40.35	26
27	40 50	40 65	40 80	40.95	41.10	41.25	41 40	41.55	41.70	41.85	27
28	42 00	42 15	42.30	42.45	42.60	42 75	42.90	43.05	43.20	43.35	28
29	43 50	43 65	43.80	43 95	44.10	44 25	44 40	44.55	44.70	44 85	29
30	45 00	45 15	45.30	45 45	45.60	45.75	45.90	46.05	46 20	46.35	30
31	46.50	46.65	46.80	46 95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48 00	48.15	48.30	48 45	48.60	48 75	48.90	49.05	49 20	49.35	32
33	49.50	49 65	49.80	49.95	50.10	50.25	50.40	50.55	50 70	50.85	33
34	51 00	51.15	51.30	51.45	51.60	51.75	51 90	52.05	52.20	52.35	34
35	52 50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54 00	54 15	54.30	54 45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55 50	55 65	55.80	55 95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57 45	57.60	57 75	57.90	58.05	58.20	58 35	38
39	58 50	58.65	58 80	58 95	59.10	59 25	59.40	59 55	59.70	59.85	39
40	60 00	60 15	60 30	60 45	60 60	60.75	60 90	61.05	61 20	61.35	40
41	61.50	61 65	61 80	61 95	62 10	62 25	62.40	62 55	62 70	62.85	41
42	63 00	63.15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64.35	42
43	64.50	64 65	64 80	64.95	65.10	65 25	65 40	65.55	65.70	65.85	43
44	66 00	66 15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67 50	67 65	67 80	67 95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69 00	69 15	69 30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70 50	70 65	70 80	70 95	71.10	71.25	71 40	71.55	71.70	71.85	47
48	72.00	72 15	72.30	72.45	72.60	72.75	72.90	73 05	73.20	73 35	48
49	73 50	73 65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURT HOUSE
CHARDON, O.
PHONE 256 X

TABLE OF INCHES REDUCED TO DECIMALS OF A FOOT.

Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.
1/16	.0052	5/16	.1094	2 9/16	.2135	3 13/16	.3177	5 1/16	.4219	6 5/16	.5260	7 9/16	.6302	8 13/16	.7344	10 1/16	.8385	11 5/16	.9427
1/8	.0104	3/8	.1146	5/8	.2188	7/8	.3229	1/8	.4271	3/8	.5313	5/8	.6354	7/8	.7396	1/8	.8438	3/8	.9479
3/16	.0156	7/16	.1198	11/16	.2240	15/16	.3281	3/16	.4323	7/16	.5365	11/16	.6406	15/16	.7448	3/16	.8490	7/16	.9531
1/4	.0208	1/2	.1250	3/4	.2292	4—	.3333	1/4	.4375	1/2	.5417	3/4	.6458	9—	.7500	1/4	.8542	1/2	.9583
5/16	.0260	9/16	.1302	13/16	.2344	1/16	.3385	5/16	.4427	9/16	.5469	13/16	.6510	1/16	.7552	5/16	.8594	9/16	.9635
3/8	.0313	5/8	.1354	7/8	.2396	1/8	.3438	3/8	.4479	5/8	.5521	7/8	.6563	1/8	.7604	3/8	.8646	5/8	.9688
7/16	.0365	11/16	.1406	15/16	.2448	3/16	.3490	7/16	.4531	11/16	.5573	15/16	.6615	3/16	.7656	7/16	.8698	11/16	.9740
1/2	.0417	3/4	.1458	3—	.2500	1/4	.3542	1/2	.4583	3/4	.5625	8—	.6667	1/4	.7708	1/2	.8750	3/4	.9792
9/16	.0469	13/16	.1510	1/16	.2552	5/16	.3594	9/16	.4635	13/16	.5677	1/16	.6719	5/16	.7760	9/16	.8802	13/16	.9844
5/8	.0521	7/8	.1563	1/8	.2604	3/8	.3646	5/8	.4688	7/8	.5729	1/8	.6771	3/8	.7813	5/8	.8854	7/8	.9896
11/16	.0573	15/16	.1615	3/16	.2656	7/16	.3698	11/16	.4740	15/16	.5781	3/16	.6823	7/16	.7865	11/16	.8906	15/16	.9948
3/4	.0625	4—	.1667	1/4	.2708	1/2	.3750	3/4	.4792	7—	.5833	1/4	.6875	1/2	.7917	3/4	.8958		
13/16	.0677	1/16	.1719	5/16	.2760	9/16	.3803	13/16	.4844	1/16	.5885	5/16	.6927	9/16	.7969	13/16	.9010		
7/8	.0729	1/8	.1771	3/8	.2813	5/8	.3854	7/8	.4896	1/8	.5938	3/8	.6979	5/8	.8021	7/8	.9063		
15/16	.0781	3/16	.1823	7/16	.2865	11/16	.3906	15/16	.4948	3/16	.5990	7/16	.7031	11/16	.8073	15/16	.9115		
1/16	.0833	1/4	.1875	1/2	.2917	3/4	.3958	6—	.5000	1/4	.6042	1/2	.7083	3/4	.8125	11—	.9167		
1/8	.0885	5/16	.1927	9/16	.2969	13/16	.4010	1/16	.5052	5/16	.6094	9/16	.7135	13/16	.8177	1/16	.9219		
3/16	.0938	3/8	.1979	5/8	.3021	7/8	.4063	1/8	.5104	3/8	.6146	5/8	.7188	7/8	.8229	1/8	.9271		
1/4	.0990	7/16	.2031	11/16	.3073	15/16	.4115	3/16	.5156	7/16	.6198	11/16	.7240	15/16	.8281	3/16	.9323		
5/16	.1042	1/2	.2083	3/4	.3125	5—	.4167	1/4	.5208	1/2	.6250	3/4	.7292	10—	.8333	1/4	.9375		

B. K. ELLIOTT COMPANY, PITTSBURG, PA.
DRAWING MATERIALS AND SURVEYING INSTRUMENTS